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## A QUANTITATIVE ASSESSMENT OF THE EFFECTS OF BASE LEVEL FALL AND BASIN DEPTH ON RIVER-DOMINATED DELTAS

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Geosciences

by

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#### Abstract

A better understanding of how deltas form and their resulting morphologic and stratigraphic characteristics is needed to improve geoscientist's abilities to manage deltas and their wetland systems as well as explore and develop hydrocarbon resources. Inherently, deltas form as shoreline regressions, making sea level cycle interpretation difficult. Here we seek to quantify the effects of relative base level fall (BLF) and basin depth on the morphology and internal geometry of river-dominated deltas in order create a model that can be applied to distinguish between deltas experiencing forced regressions and normal regressions. Doing so will allow us to more accurately interpret the sequence stratigraphic record. We propose measuring the relative influence of BLF and basin depth on delta formation through the shoreline trajectory. The shoreline trajectory is defined as the locus of points defined by the shoreline in the vertical plane. We find that as basin depth increases, the number of active distributaries decreases because river mouth bars take longer to aggrade leading to fewer bifurcations. Increased basin depth increases the avulsion period because it takes longer for enough sediment to be deposited such that a distributary channel becomes super-elevated and can avulse. Fewer active distributaries and longer avulsion periods lead to deposition being focused in one region for greater periods of time which results in more rugose shorelines and more variability in foreset dip directions. Deeper basin depths are associated with smaller average lobe areas because more sediment is required to form a lobe of equal areal extent in a deep basin than in a shallow basin. We find that the greater volume of sediment required in deeper basins outweighs the more focused deposition also associated with a deeper basin, thereby forming smaller delta lobes on average. We find that the thickness of topset

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deposits varies little with basin depth while the foreset thickness varies greatly. This leads to decreased volumetric topset/foreset ratios in deeper basins. Deeper basins have delta fronts that are less affected by tractional sediment transport resulting in larger clinoform average dip magnitudes. Higher rates of BLF results in elongate a deltas with greater topset roughness caused by down-stepping lobes. Higher rates or BLF are also associated with larger total topset areas. Twelve deltas simulated deltas are formed under different rates of BLF and basin depths using Delft3D, an engineering-grade, 2D vertically integrated hydrodynamic and morphodynamic model. The model is an improvement over earlier models because it accounts for multiple grain size fractions, cohesive sediment fractions, and bed stratigraphy. The model findings are validated with data collected from the Goose River Delta, sandy, fjord-style delta prograding into the 30m deep basin of Goose Bay, Labrador, Canada and experiencing 5 mm of BLF per year for the last 8000 years. A re-interpretation of the Cretaceous Panther Tongue Member of the Starr Point Formation in the Book Cliffs of Utah, USA is based on clinoform dip and dip direction variability data. We propose that the southern lobe of the Panther Tongue Delta, near Crandall Canyon, has higher clinoform dips due to it prograding into deeper water as opposed to BLF because clinoform heights increase from proximal (north) to distal (south) indicating deeper water depths in the south.

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- 1 Introduction
- 2

3 A better understanding of how deltas form and their resulting morphologic and stratigraphic

4 characteristics is needed to improve geoscientist's abilities to manage deltas and their wetland systems

5 as well as explore and develop hydrocarbon resources. To this end we seek to improve current

6 predictive tools by modeling deltas forming under varying rates of base level fall and initial basin

7 depths, validating model results with the modern Goose River Delta in Labrador, Canada which is

8 experiencing 5 mm yr<sup>-1</sup> of base level fall, and applying validated model results to the Panther Tongue

9 Member of the Star Point Formation near Helper, Utah as a case study.

Sequence stratigraphy has become the de facto predictive tool for interpreting the relationships between facies successions and base level changes, yet much work must still be done to fully quantify these relationships. At the heart of sequence stratigraphy is the balance of sediment supply and the change in accommodation, and deltas represent an environment where this balance is inherently complex. Quantification of how deltas form in different base level conditions will help refine sequence stratigraphic principles for these complex systems and create a more robust predictive tool.

## 16 Background

There are two contrasting views on how relative base level fall (BLF) affects deltas. Some researchers
think that BLF causes deltas to elongate and develop incised valleys because lateral migration of
channels and avulsions are suppressed (Suter and Berryhill 1985; Sala and Long 1989; Corner et al.,
1990; Walker 1992; Posamentier and Allen 1992a; Posamentier and Allen 1992b; Hart and Long 1996;
Posamentier and Morris 2000; Howell and Flint 2003; Porebski and Steel 2003; Porebski and Steel
2006). Whereas others think deltas can remain in an aggradational regime during BLF such that their
planforms and stratigraphies give no indication that accommodation space is decreasing (Muto and Steel

24 2004; Muto and Swenson 2005; Muto and Swenson 2006; Swenson and Muto 2007; Petter and Muto
25 2008; Lorenzo-Trueba et al. 2013; Prince and Burgess 2013).

26	The former view arose in early conceptual stratigraphic models of deltas. Falling base level was
27	thought to form elongate deltas with incised valleys and suppressed lobe and channel switching (Walker
28	1992; Posamentier and Allen 1992a), and create channelized sediment bypass zones cutting across older
29	delta lobes (Fig.1) (Posamentier and Allen 1992a; Posamentier and Allen 1992b). Later workers
30	modified this view, arguing that the formation of incised valleys was confined to shelf-edge deltas (Suter
31	and Berryhill 1985; Porebski and Steel 2003; Porebski and Steel 2006). Posamentier and Morris (2000)
32	and later Howell and Flint (2003) formalized these earlier ideas in a set of 8 characteristic features that
33	should be seen in the stratigraphic record for both inner-shelf and shelf-edge, forced-regressive deltas
34	(i.e., deltas subject to BLF, also referred to as falling-stage deltas):
35	1) presence of a significant zone of lateral separation between successive shoreface deposits;
36	2) sharp-based shoreface/delta front deposits;
37	3) progressively lower relief clinoforms going from proximal to distal;
38	4) occurrence of long-distance regression;
39	5) absence of fluvial and/or coastal plain/delta plain facies capping the proximal portion of
40	regressive deposits;
41	6) presence of a seaward-dipping upper bounding surface;
42	7) increased average sediment grain size in regressive deposits going from proximal to distal due to
43	lack of accommodation for coarse grains on the topset; and
44	8) presence of "foreshortened" stratigraphic successions where the measured thickness of
45	parasequences is considerably less than estimates of paleowater depth (i.e., there is a subaqueous

- 46 clinform rollover some distance away from the shoreline), suggesting coeval relative sea-level47 fall.
- 48 Based upon these criteria, both Posamentier and Morris (2000) and Howell and Flint (2003) argued that
- 49 the Panther Tongue Mbr. of the Starr Point Fm. near Helper, UT, USA is a forced-regressive delta.



Figure 1. Early conceptual models suggested that BLF forms elongate deltas with down-stepping lobes,
incised valleys, and suppressed lobe and channel switching, as well as creates channelized sediment
bypass zones cutting across older delta lobes. Dotted lines indicate the delta front.

- 54 Studies of modern deltas in areas of glacial rebound generally supported this earlier view of delta
- response to BLF (Corner et al., 1990; Sala and Long, 1989; Hart and Long, 1996). Researchers pointed
- 56 out their terraced paleoshorelines, abandoned delta lobes, and distributary incision (Hart and Long
- 57 1996). The latter prevents lateral fluvial erosion of the topset until base level begins to rise during early

lowstand. This observation suggests that criterion 5 of Posamentier and Morris (2000) is likely the
result of subsequent base level rise rather than occurring during BLF.

60 That deltas can remain in an aggradational regime during BLF was first suggested by numerical 61 and physical models. Muto and Steel (2004) formed unscaled flume deltas experiencing varying 62 dimensionless base level fall rates, water discharge to sediment discharge ratios, and basin slope. They 63 found that numerical and experimental deltas experiencing BLF remain aggradational until an intrinsic 64 response time has been met, at which time the first major incision of the distributary channels form. Muto and Steel (2004) called this type of downcutting "auto-incision." The intrinsic response time,  $\tau$ 65 (yr), was defined by Swenson and Muto (2007) as  $\tau = \frac{q_{s0}^2}{v} |\dot{r}|^{-2}$  where  $q_{s0}$  is the sediment supply (m<sup>2</sup> yr<sup>-</sup> 66 <sup>1</sup>),  $\dot{r}$  is the rate of BLF (m yr<sup>-1</sup>), and v is the fluvial diffusivity (m<sup>2</sup> yr<sup>-1</sup>). The intrinsic response time 67 68 represents a threshold time at which point the channel abandons its former floodplain and incises due to 69 continued steady BLF. Prior to this time the delta continues to prograde seaward and as a consequence. 70 the whole channel network up to the mountain front must aggrade to maintain its energy slope. Thus the 71 alluvial-bedrock transition migrates progressively landward and the alluvial plain continues to rise, even 72 after the initiation of BLF. After the intrinsic response time, a wave of incision sweeps up the system. 73 Rivers then reach grade, or create a sediment bypass zone in which no net erosion or deposition is 74 occurring, if the rate of BLF varies with the square root of time (Muto and Steel 2005). This behavior 75 arises as the result of the linearly sloping basin used in their experiment which causes the shoreline and 76 delta-toe to advance basinward at a constantly decreasing rate. Muto and Swenson (2006) built upon 77 this work and found that rivers can attain grade via an autogenic response to steady BLF, regardless of 78 the rate of BLF, if the initial basin slope is the same as the slope of the graded reach. In that study, the 79 authors conducted flume experiments fed only with sand to form deltas. These flume experiments were 80 unscaled in that they did not account for Froude-scaling. This study contradicts Muto and Steel's (2005) theory that base level fall must vary with the square root of time in order for a river to attain grade. In a numerical modeling and unscaled flume experiment, Swenson and Muto (2007) determined that deltas are unable to attain grade while experiencing steady BLF and actually remain aggradational until the intrinsic response time is reached, and then the deltas become incisional. Lorenzo-Trueba et al. (2013) use a geometric, mass-balance model that treats the shoreline and the alluvial-bedrock transition as moving boundaries to support the idea that BLF is not a sufficient condition for incision.

87 The studies summarized above underscore the roles played during BLF by the relative 88 magnitudes of the initial fluvial slope and the basin floor slope. If the fluvial slope is greater than the 89 slope of the receiving basin, the alluvial river aggrades faster during BLF, resulting in sediment 90 starvation of its delta and retreat of the delta shoreline. Petter and Muto (2008) called this phenomenon 91 "auto-detachment." Petter and Muto (2008) observed "auto-detachment" in an unscaled flume 92 experiment and a diffusion-based forward numerical model in which cohesive sediment was ignored. 93 Even the characteristic features in the list above may not be indicative of forced regressive deltas. 94 Prince and Burgess (2013) report that topset/foreset ratios are not indicative of BLF and are non-unique. 95 They arrived at this conclusion by conducting numerical experiments using the diffusion-based 96 numerical model, named Dionisos, in which they varied the rate of BLF and the basin slope. 97 In summary, there are two contrasting views on delta response to BLF. Some workers argue that 98 deltas experiencing BLF will become elongate and incised, whereby lateral channel migration and 99 distributary avulsions are suppressed (Suter and Berryhill 1985; Sala and Long 1989; Corner et al., 100 1990; Walker 1992; Posamentier and Allen 1992a; Posamentier and Allen 1992b; Hart and Long 1996; 101 Posamentier and Morris 2000; Howell and Flint 2003; Porebski and Steel 2003; Porebski and Steel 102 2006). On the other hand, others argue that falling-stage deltas will remain aggradational for a time, and 103 then experience a variety of phenomena including graded, "auto-incision", and "auto-detachment".

This varied response may produce non-unique stratigraphies (Muto and Steel 2004; Muto and Swenson
2005; Muto and Swenson 2006; Swenson and Muto 2007; Petter and Muto 2008; Lorenzo-Trueba et al.
2013; Prince and Burgess 2013).

107 The effects of water depth on delta morphology and internal geometry have been typically 108 considered by categorizing deltas from shallowest to deepest as bayhead, inner shelf, mid-shelf, and 109 shelf-margin deltas (Porebski and Steel, 2006). Conceptual models (Porebski and Steel 2006, Kolla et 110 al. 2000) predict that bayhead deltas will possess many distributaries, be river-dominated, and be 111 confined and funnel-shaped. Inner-shelf deltas are commonly thought to have shallow clinoform slopes 112 (Reading and Collison 1996) and to fall within the Galloway et al. (1975) tripartite regime of river-, 113 wave-, and tide dominated deltas. Mid-shelf deltas are predicted to possess steeper clinoforms 114 (Posamentier and Morris 2000), and be either river- or wave- dominated. Porebski and Steel (2006), 115 Kolla et al. (2000) suggested that mid-shelf deltas are often associated with BLF and therefore should 116 have thin to absent topsets due to incision during BLF. It is unclear whether the authors recognize any 117 mid-shelf deltas that are not experiencing BLF. Shelf-margin deltas are thought to be elongate deltas 118 that possess the steepest clinoforms (Porebski and Steel 2006, Kolla et al. 2000). In summary, 119 conceptual models predict that shelf-margin deltas in deep water will become more elongate and form 120 steeper clinoforms than shallow-water, bayhead and inner-shelf deltas. It is important to note that many 121 conceptual models are underlain by sequence stratigraphic logic which tends to conflate basin depth and 122 rate of BLF, failing to acknowledge that deltas may prograde into deep-water without regard to the rate 123 of base level rise or fall.

124 The goal of this paper is to help resolve these debates by quantifying the effect of varying rates 125 of relative base level fall and basin depths on the planform and internal geometry of properly scaled 126 deltas formed with multiple grain size fractions and cohesive sediments. Quantification allows for a

better understanding of the relative influence of different amounts of forcings on delta planforms and
internal geometries. Consequently, our quantification provides a more widely applicable predictive tool
for the interpretation of deltas experiencing BLF.

### 130 Statement of the Problem

Previous studies have focused on either the morphology of modern systems (Sala and Long 1989; 131 132 Corner et al. 1990; Hart and Long 1996), the stratigraphy of ancient systems (Suter and Berryhill 1985; 133 Walker 1992; Posamentier and Allen 1992a; Posamentier and Allen 1992b; Posamentier and Morris 134 2000; Howell and Flint 2003; Porebski and Steel 2003; Porebski and Steel 2006), or in some cases 135 highly simplified modeling of both (Muto and Steel 2004; Muto and Swenson 2005; Muto and Swenson 136 2006; Swenson and Muto 2007; Petter and Muto 2008; Lorenzo-Trueba et al. 2013; Prince and Burgess 137 2013). Here we hope to better understand delta response to falling base level and basin depth by using 138 Delft3D modelling. No previous modelling study has thus far been a 2D vertically-averaged flow model 139 accounting for multiple grain sizes, cohesive sediment, and bed stratigraphy, so this paper represents a 140 significant improvement over previous models. Here, we define base level fall as any relative drop in sea 141 or lake level, regardless of the origin of the relative fall. We attempt to answer two questions: 1) when 142 and under what conditions of base level fall rate and basin depth will a delta switch from progradation 143 and aggradation to downstepping and degradation; and 2) what morphological features and internal 144 geometries if any, are characteristic of a falling-stage delta?

A useful non-dimensional parameter incorporating both BLF and basin depth is the shoreline
trajectory, S<sub>T</sub>:

$$S_T = \frac{\dot{r}}{PR'},\tag{1}$$

147 where  $\dot{r}$  is the rate of relative base level fall (mm yr<sup>-1</sup>) and PR is the time-averaged progradation rate of 148 the delta (mm yr<sup>-1</sup>) spatially averaged over the delta perimeter, defined as

$$PR = (A/P)/t \tag{2}$$

where A equals topset area  $(mm^2)$ , P equals delta shoreline length (mm), and *t* is time (yr). Note that if the rates of BLF and sediment fluxes of two deltas are equal, then the progradation rate is set solely by the basin depth.

152 We hypothesize that deeper initial basin depths will result in fewer active distributaries, longer 153 avulsion periods, a more rugose shoreline, greater foreset dip azimuth variability, larger clinoform dip 154 magnitudes, lower topset/foreset ratios, and smaller average delta lobe areas while higher rates of base 155 level fall should result in greater topset roughness. We predict that deeper initial basin depth will result 156 in longer time periods for river mouth bars to aggrade to a height at which they can bifurcate 157 distributaries which in turn causes fewer active distributaries. With deeper initial basin depths channels 158 must aggrade more in order to become super-elevated and avulse, therefore longer time periods are 159 required for a channel to become super-elevated and avulse. This process results in an increased 160 avulsion period. Fewer active distributaries and longer avulsion periods should focus sediment 161 deposition in fewer locations for longer periods of time thereby creating irregular, rugose shorelines. 162 Based on this logic we expect deltas with deeper initial basin depths to have more rugose shorelines than 163 deltas forming in shallow basins. The more focused deposition associated with deeper initial basin 164 depths should also result in reduced foreset dip azimuth variability. Delta lobes in deeper basins require 165 more sediment per unit of area; therefore deeper basin depths should result in smaller delta lobe areas on 166 average. Deeper basin depths result in tractional sediment transport occurring over a smaller portion of 167 the delta front than in shallower basins. Tractional sediment transport tends to create shallower 168 clinoform slopes than suspended transport; therefore we expect deeper initial basin depths to result in 169 tractional transport accounting for less of the total sediment transport along the delta front and larger 170 clinoform dip magnitudes. We predict that deeper basins will result in lower topset/foreset ratios

because while the thickness of topset deposits, set by the height of levees and point bars in distributary channels, should be relatively constant across basin depths, the foreset thicknesses must be larger in deeper basins. Higher rates of BLF should have lobes that downstep by larger amounts leading to greater topset roughness. In contrast to Posamentier and Morris (2000), we expect no change in mean grain size across delta lobes from proximal to distal because any change in the amount of coarse-grained sediment in the total sediment load of a given distributary channel should be small in relation to the total sediment load delivered to that distributary channel by the main channel feeding the delta.

178 Our approach is to build deltas under various boundary conditions using Delft3D, a high-179 complexity numerical model often used in engineering studies, and perform an in-depth validation study 180 of the model by testing those model predictions against morphological and stratigraphical data from the 181 modern Goose River Delta, Labrador where relative base level has fallen at the rate of at least 5 mm yr<sup>-1</sup> 182 over the last 7,000 yrs. We then attempt to better understand the origin of the Panther Tongue Member 183 of the Starr Point Formation near Helper, UT, USA using the results of the modeling study. This 184 approach allows us to validate model predictions with a modern delta and test those predictions against a 185 delta in the rock record as a case study.

The rest of this paper is structured such that it brings the reader through the model development, validation, and application. To this end, the variables of interest will first be defined. The Delft3D modelling approach and methods will be described, followed by model results and a discussion of their significance. Next, an overview of the Goose River Delta and the methods employed to study it will be presented, followed by results from the Goose River Delta. A discussion of the Goose River Delta validation study will follow. Validated model results will then be applied to the Panther Tongue Member as a case study. Finally, the key findings and conclusions of this study will be presented.

## 193 Variables

- 194 Nine variables (Fig. 2) are used to characterize deltas in this study: (1) number of active distributaries,
- 195 (2) avulsion period, (3) shoreline rugosity, (4) foreset dip-azimuth uniformity statistic, (5) average
- 196 clinoform dip magnitude, (6) topset/foreset thickness ratio, (7) topset roughness, (8) coefficient of
- 197 determination for degree of coarsening or fining of delta lobes from oldest to youngest, and (9) the
- 198 average delta lobe subaerial area. These variables were chosen to characterize the general planform and
- stratigraphy of because they are process-focused, and test existing conceptual models of deltas
- 200 experiencing BLF.



## 203

**Figure 2.** In the schematic delta above, there are four active distributaries; therefore N = 4. The shoreline rugosity is defined as  $R=P^2/4\pi A$ , where P is the topset perimeter (highlighted in yellow) and A is the topset area (the area within the yellow polygon). Clinoform dip magnitudes,  $\phi$ , are averaged across the whole delta foreset. The dip azimuths at grid points on the foreset are used to compute the foreset dip azimuth variance,  $\overline{R}$ . The topset roughness, X, is defined as the standard deviation of surface elevations within the yellow polygon.

210

211 The number of active distributaries in the modeled deltas, N, is defined as the time-averaged

number of simultaneously active distributaries that are at least 50 m wide at their widest point and have

a depth-averaged flow velocity greater than  $0.8 \text{ m s}^{-1}$ .  $0.8 \text{ m s}^{-1}$  is the flow velocity that allows the user

- to clearly differentiate between overland and channelized flow in the Delft3D models. Flow velocities
- less than 0.8 m s<sup>-1</sup> are commonly associated with overland flow or small distributaries. For the modern
- 216 Goose River Delta, we counted distributaries that were at least 50 m wide at their widest point in aerial

photographs taken in 1951, 1970, 1975, 1987, 1998, and 2012. Values from each year were given equal
weight and averaged. No flow velocity criterion was used. This variable could not be measured in the
Panther Tongue Delta. The number of active distributaries is of interest because it is a strong control on
a number of other delta morphometries including shoreline rugosity.

221 The avulsion period, T, is defined as the average recurrence interval for major avulsions or 222 channel reoccupations of former channels. A major avulsion is defined operationally as a shift in locus 223 of deposition of more than 5 channel widths (i.e., a lobe switching event). For the modeled deltas the 224 intervals between avulsions were noted and averaged. We calculated the avulsion period for the Goose 225 River Delta by dividing the number of identifiable, active, and abandoned lobes by the time it took to 226 form the identified lobes. We identified five lobes, and were able to determine the duration of lobe 227 formation from radiocarbon dates. Avulsion period was not measured in the Panther Tongue Mbr. The 228 avulsion period is important because it dictates how long sediment deposition is focused at one location 229 and therefore the shape of the delta.

Shoreline rugosity is measured in the model simulations and the modern Goose River Delta
following Burpee et al. (in review). The shoreline rugosity, R, is defined as:

$$R = P^2 / 4\pi A \tag{3}$$

where P is the delta's shoreline perimeter (km) and A is the delta's topset area (km<sup>2</sup>). Higher values of R correspond to more complex shorelines. The shoreline is delineated in the modeled deltas using the open angle method with a threshold angle of 25° (Shaw et al. 2008). For the Goose River Delta, the shoreline of the whole delta complex, including paleoshorelines of abandoned lobes, was delineated by interpreting aerial photographs and a digital elevation model. Shoreline rugosity was not measured in the Panther Tongue Mbr. Shoreline rugosity is a valuable statistic because it gives a sense of how the delta is shaped which could be useful in delta management and oil and gas exploration. Foreset dip azimuth variance,  $\overline{R}$ , is measured by calculating the length of the mean resultant vector from the azimuthal data and normalizing for the number of samples (Jones 2006). The length of the resultant vector, *R*, is defined by:

242

$$R = \sqrt{X^2 + Y^2} \tag{4}$$

243 where X and Y are the summed x and y components (L) of each foreset dip azimuth, respectively.  $\overline{R}$  is 244 defined as:

$$\bar{R} = R/N \tag{5}$$

where N is the sample size.  $\overline{R}$  varies between 0-1. A value of 1 means that the length of the resultant vector length is equal to the sample size indicating the foreset dip azimuths have little variance and are all oriented in the same direction. A value of 0 indicates a large variance in foreset dip azimuths with the vectors oriented more equally around the compass. The foreset dip azimuth variance provides insight into both how complex the delta front is (a low  $\overline{R}$  value) and how elongate a delta is (a high  $\overline{R}$ value) (Fig. 3).





Figure 3. Foreset dip azimuth variance increases ( $\overline{R}$  decreases) from A to C. Elongate deltas (A) have less variance in foreset dip azimuths with most dips oriented perpendicular to the direction of progradation. Fan deltas (B) have a moderate amount of variance in foreset dip azimuths, but tend not to have any azimuths in oriented in the southern hemisphere (90° - 270°). Irregularly-shaped deltas (C) have the most variability in foreset dip azimuths because they have dips oriented equal proportion around the entire compass (0°-360°).

258	Aspect ratio is measured to convey a sense of how elongate a delta is. The aspect ratio is defined
259	as the ratio between the width of the delta perpendicular to the main channel and the length of the delta
260	from proximal to distal. The width and length are measured by fitting a rectangle to the shoreline of the
261	delta such that the most extreme locations in each direction are just encompassed by the rectangle (Fig.
262	4). A high aspect ratio indicates that the delta does not extend very far into the basin, but rather extends
263	parallel to the pre-existing beach. A low aspect ratio indicates an elongate delta prograding far into the
264	basin in relation to its width and could be useful for hydrocarbon exploration





265

269 The average clinoform dip magnitude,  $\phi$ , is the spatially averaged true dip taken from the surface 270 of a clinoform. Clinoform dips magnitudes from the model simulations were calculated from the 271 clinoform at the last timestep by extracting the bed slope at each 25 m x 25 m grid point within the 272 foreset region. The foreset is defined as the region between the topset and bottomset (Gilbert 1885). 273 The extent of the foreset was defined as all elevations below -0.1 m MSL down to the clinoform toe 274 where the dip magnitude became less than  $0.008^{\circ}$ . It should be noted that Delft3D does not simulate 275 foreset slumping or turbidity currents. Therefore the dip magnitude in the model is expected to be 276 higher on average than would be found in nature. For the Goose River Delta, the average clinoform dip 277 magnitude was taken from a multibeam bathymetry survey of the southern active delta lobe. The 278 multibeam bathymetry point data were interpolated into a raster in ArcGIS. Slopes were calculated from 279 the raster using Arc Toolbox. The foreset region was extracted and averaged in the same fashion as for

280 the Delft3D simulations. Clinoform dips were gathered from the Panther Tongue using a laser ranger to 281 measure two trends and plunges of foresets on two faces with differing bearings. The attitude of the 282 resulting bed was then corrected for tectonic dip. Locations of these measurements are shown in Figure 283 5. These data were gathered throughout the extent of the Panther Tongue Mbr. outcrop belt, but these 284 stratigraphic data are inherently less representative of the ancient system than the model and modern 285 delta data. Clinoform dip magnitudes are easily measurable in the field and in seismic line and could be 286 inverted to help determine the basin depth and rate of BLF that were influencing a delta's formation. 287 Topset roughness, X, is defined as the standard deviation of topset elevations that are greater 288 than 0 m above MSL. Edmonds and Slingerland (2010) conjectured that this variable should be 289 correlated with the avulsion period because high channel levees that should suppress avulsions also 290 increase the topset roughness. Topset roughness was extracted from the Delft3D deltas by calculating 291 the standard deviation of elevations taken every 25 m that were greater than the final base level. Topset 292 roughness was measured on the Goose River Delta from dGPS points taken at random intervals along a 293 strike line across the delta. The topset of Panther Tongue Delta has been removed by subsequent 294 erosion and was not measured. Topset roughness is a good indicator of the degree of down-stepping that 295 has occurred.

Proximal to distal trends in delta grain size for the Delft3D simulations were measured as a rate of fining, G. The average grain size of each delta lobe in a simulation was approximated using the D50 of 100 representative cells of each lobe each 0.1 m thick x 25 x 25 m. The D50 of each lobe was then regressed against distance from the delta apex to the toe of the delta lobe. The slope of the regression line corresponds to G. A large value of G indicates a large rate of fining in delta lobes from proximal to distal across the whole delta. This variable was not measured for the Goose River Delta. Grain sizes were measured in outcrops of the Panther Tongue, although not enough data regarding the number,

303	position, and age of lobes were available to perform a meaningful correlation. Mean grain size could be
304	inverted to determine the basin depth and rate of BLF conditions in which a delta formed.
305	Average delta lobe area, A, in the Delft3D simulations is defined as the areal extent of the topset
306	for each lobe at the time of abandonment. The shoreline was defined as the 0 m MSL contour separating
307	the subaerial and subaqueous portions of the delta. The 0 m MSL contour was not traced into
308	distributary channels. Delta lobes in the Goose River Delta were delineated and measured using a
309	digital elevation model and aerial photographs. This variable was not measured for the Panther Tongue
310	Delta. Average lobe size would be useful for hydrocarbon exploration.



311

111°0'0"W

Figure 5. Clinoforms in the Panther Tongue Mbr. of the Starr Point Fm. were measured using a laser ranger at the locations indicated above. The red outlines the Panther Tongue Mbr. outcrop belt.

## 314 Numerical Experiments

## 315 Model Description

- 316 We simulated 12 river deltas using Delft3D, a physics-based, fluid flow and sediment transport model
- for modeling morphodynamic systems at time scales of minutes to hundreds of years (e.g., Storms et
- al.,2007; Edmonds and Slingerland, 2010; Canestrelli et al., 2013; Caldwell and Edmonds, 2014; van der
- 319 Vegt et al., 2014). The software solves the Navier-Stokes equations for an incompressible fluid and
- 320 makes use of the shallow water and Boussinesq assumptions.
- 321 Hydrodynamics
- We used Delft 3D in its 2-D depth-averaged mode in which  $u_x$  and  $u_y$ , the x- and y-directed flow
- 323 velocities (m s<sup>-1</sup>), are obtained from the depth-averaged conservation of momentum equations for a
- 324 homogeneous fluid,

$$\frac{\partial u_x}{\partial t} + u_x \frac{\partial u_x}{\partial x} + u_y \frac{\partial u_x}{\partial y} + f u_y = -\frac{1}{\rho} \frac{\partial P}{\partial x} + \frac{\tau_{sx} - \tau_{bx}}{\rho(d+\zeta)} + F_{u_x}$$
(6)

$$\frac{\partial u_y}{\partial t} + u_x \frac{\partial u_y}{\partial x} + u_y \frac{\partial u_y}{\partial y} - f u_x = -\frac{1}{\rho} \frac{\partial P}{\partial y} + \frac{\tau_{sy} - \tau_{by}}{\rho(d+\zeta)} + F_{u_y}$$
(7)

where *P*, *f*,  $\rho$ ,  $\zeta$  and *d* are the fluid pressure (N m<sup>-2</sup>), Coriolis parameter (s<sup>-1</sup>), fluid density (kg m<sup>-3</sup>), water level above a reference plane (m), and the water depth below the reference plane (m), respectively. *Fu<sub>x</sub>* and *Fu<sub>y</sub>* are the x- and y- directed horizontal Reynold's stresses (m s<sup>-2</sup>),  $\tau_{sx}$  and  $\tau_{sy}$  are the x- and ydirected shear stresses (N m<sup>-2</sup>) at the water surface (set to zero in these experiments), while  $\tau_{bx}$  and  $\tau_{by}$ are the x- and y-directed shear stresses (N m<sup>-2</sup>) at the bed. The bed shear stresses are calculated as,

$$\frac{\tau_{bx}}{\rho} = c_f u_x \sqrt{u_x^2 + u_y^2} \tag{8}$$

$$\frac{\tau_{by}}{\rho} = c_f u_y \sqrt{u_x^2 + u_y^2} \tag{9}$$

330 where  $c_f$  is the dimensionless Chezy friction factor.

331 The continuity equation for water is computed as,

$$\frac{\partial\zeta}{\partial t} + \frac{\partial[(d+\zeta)u_x]}{\partial x} + \frac{\partial[(d+\zeta)u_y]}{\partial y} = Q$$
(10)

332 where Q (m s<sup>-1</sup>) is the contribution per unit area due to the discharge or withdrawal of water,

333 precipitation, and evaporation.

The x- and y-directed horizontal Reynold's stresses,  $F_U$  and  $F_V$ , are computed using a horizontal large eddy simulator in which the horizontal eddy viscosity is defined as:

$$v_H = v_{SGS} + v_H^{back} \tag{11}$$

336 where  $v_H$  is the horizontal eddy viscosity (m<sup>2</sup> s<sup>-1</sup>),  $v_{SGS}$  is the contribution from the sub-grid scale

horizontal eddy viscosity modeled with the HLES (m<sup>2</sup> s<sup>-1</sup>), and  $v_H^{back}$  is the user-defined background

horizontal eddy viscosity  $(m^2 s^{-1})$ . Similarly, the horizontal eddy diffusivity is calculated as:

$$D_H = D_{SGS} + D_H^{back} \tag{12}$$

339 where  $D_H$  is the total horiztonal eddy diffusivity coefficient (m<sup>2</sup> s<sup>-1</sup>),  $D_{SGS}$  the contribution from the sub-

340 grid scale horizontal eddy viscosity modeled with the horizontal large eddy simulation technique

341 (HLES), and  $D_H^{back}$  is the user-defined background horizontal eddy viscosity (m<sup>2</sup> s<sup>-1</sup>). The effect of sub-

342 grid scale turbulence on the horizontal viscosity coefficient is computed using Uittenbogaard and van

343 Vossen's (2004) HLES technique in which  $v_{SGS}$ , the sub-grid eddy viscosity (m<sup>2</sup> s<sup>-1</sup>), is given by:

$$\nu_{SGS} = \frac{1}{k_s^2} \left( \sqrt{(\gamma \sigma_T S^*)^2 + B^2} - B \right) \tag{13}$$

344 with:

$$B = \frac{3g|u_x|}{4HC^2} \tag{14}$$

345 where  $k_s$  is the truncation wave number (m<sup>-1</sup>),  $\gamma$  is a dimensionless coefficient relating the spectral 346 energy density to the wave number,  $\sigma_T$  is the dimensionless Prandtl-Schmidt number, and  $S^*$  (s<sup>-1</sup>) is the 347 strain rate tensor based upon the low, then high pass filtered, computationally resolved, horizontal

- 348 velocity vector  $\underline{U}$  (m s<sup>-1</sup>), B is a damping bed friction term (s<sup>-1</sup>), C is the Chezy friction coefficient (m<sup>1/2</sup>s<sup>-1</sup>)
- 349 <sup>1</sup>), and H is the total water depth (m).
- 350 The sub-grid scale eddy diffusivity for the mixing of mud is:

$$D_{SGS} = \frac{\nu_{SGS}}{\sigma_T} \tag{15}$$

351

- 352 Sediment Transport
- 353 After the hydrodynamic equations are solved, sediment transport is computed. In Delft3D silt- and clay-
- 354 sized particles are called cohesive. Both cohesive and non-cohesive suspended sediment transport are
- 355 computed using the depth-averaged 3D advection-diffusion equation:

$$\frac{\partial c_i}{\partial t} + \frac{\partial u_x c_i}{\partial x} + \frac{\partial u_y c_i}{\partial y} + \frac{\partial (u_z - w_{s,i}) c_i}{\partial z} = \frac{\partial}{\partial x} \left( \varepsilon_{s,x,i} \frac{\partial c_i}{\partial x} \right) + \frac{\partial}{\partial y} \left( \varepsilon_{s,y,i} \frac{\partial c_i}{\partial y} \right) + \frac{\partial}{\partial z} \left( \varepsilon_{s,z,i} \frac{\partial c_i}{\partial z} \right)$$
(16)

where  $c_i$  is the mass concentration of the *i*th sediment fraction (kg m<sup>-3</sup>), *u*, *v*, and *w* are flow velocity components (m s<sup>-1</sup>), and  $\varepsilon_{s,x,i}$ ,  $\varepsilon_{s,y,i}$ , and  $\varepsilon_{s,z,i}$  are the eddy diffusivities of the *i*th sediment fraction (m<sup>2</sup> s<sup>-1</sup>). Non-cohesive settling velocities are computed using a Van Rijn (1993) formulation,

359

$$w_{s,i} = \begin{cases} \frac{RgD_i^2}{18\nu}, & 65\,\mu m < D_i < 100\,\mu m \\ \frac{10\nu}{D_i} \left( \sqrt{1 + \frac{0.01RgD_i^3}{\nu^2} - 1} \right), & 100\,\mu m < D_i < 1000\,\mu m \\ 1.1\sqrt{RgD_i}, & 1000\,\mu m < D_i \end{cases}$$
(17)

where  $w_{s,i}$  is the settling velocity of the *i*th sediment fraction,  $R = \rho_s / \rho_w - I$  is the submerged specific gravity,  $\rho_s$  is the specific density of sediment (kg m<sup>-3</sup>),  $\rho_w$  is the specific density of water (kg m<sup>-3</sup>), g is the acceleration due to gravity (m s<sup>-2</sup>),  $D_i$  is the grain size of the *i*th sediment fraction (m), and v is the kinematic viscosity coefficient of water (m<sup>2</sup> s<sup>-1</sup>) (*cf.*, Caldwell and Edmonds, 2014). 364

The exchange of sediment from suspension to the bed, and vice versa, is modeled by calculating,

$$-w_{s,i}c_i - \varepsilon_{s,z,i}\frac{\partial c_i}{\partial z} = D_i - E_i = T_{d,i}, at \ z = z_b$$
<sup>(18)</sup>

where  $D_i$  is the sediment deposition rate of the *i*<sup>th</sup> sediment fraction (m s<sup>-1</sup>),  $E_i$  is the sediment erosion rate of the *i*<sup>th</sup> sediment fraction (m s<sup>-1</sup>),  $T_{d,i}$  is the net deposition or erosion rate of the *i*<sup>th</sup> sediment fraction (m s<sup>-1</sup>), and  $z_b$  is the elevation of the bed (m).

368 Delft3D computes erosion and deposition of cohesive sediment using the Partheniades-Krone 369 formulation (Partheniades, 1965),

$$S_{e,i} = \begin{cases} \left(\frac{\tau_0}{\tau_{ce(C)}} - 1\right), & \text{when } \tau_0 > \tau_{ce(C)} \\ 0, & \text{when } \tau_0 \le \tau_{ce(C)} \end{cases} \end{cases}$$

$$S_{d,i} = w_{s,i} c_{b,i} \begin{cases} \left(\frac{\tau_0}{\tau_{cd(C)}} - 1\right), & \text{when } \tau_0 < \tau_{cd(C)} \\ 0, & \text{when } \tau_0 \ge \tau_{cd(C)} \end{cases}$$

$$(19)$$

where  $S_{e,i}$  is the erosion function for the *i*<sup>th</sup> sediment fraction (kg m<sup>-2</sup> s<sup>-1</sup>),  $S_{d,i}$  is the deposition function for the *i*<sup>th</sup> sediment fraction (kg m<sup>-2</sup> s<sup>-1</sup>),  $\tau_0$  is the bed shear stress (N m<sup>-2</sup>),  $\tau_{ce(C)}$  is the user-defined critical shear stress for erosion (N m<sup>-2</sup>),  $\tau_{cd(C)}$  is the user-defined critical shear stress for deposition (N m<sup>-2</sup>), and  $c_{b,i}$  is the average sediment concentration of the *i*<sup>th</sup> sediment fraction in the near bottom computational layer (kg m<sup>-3</sup>).

Bedload transport is computed using a Van Rijn (1993) formulation,

$$q_{b,i} = 0.006 w_{s,i} D_i \left( \frac{u (u - u_{c,i})^{1.4}}{(RgD_i)^{1.2}} \right)$$
(20)

where  $q_{b,i}$  is the bedload sediment discharge per unit width of the *i*<sup>th</sup> sediment fraction (m<sup>2</sup> s<sup>-1</sup>), *u* is the depth-averaged flow velocity (m s<sup>-1</sup>), and  $u_{c,i}$  is the critical depth-averaged flow velocity for entrainment of the *i*<sup>th</sup> sediment fraction based upon the Shields curve (m s<sup>-1</sup>). Bed elevation changes are calculated using a modified Exner equation with a user-definedmorphological acceleration factor

$$\left(1 - \varepsilon_{por}\right)\frac{\partial z_b}{\partial t} = -f_{MORFAC}\frac{\partial S_x}{\partial x} - \frac{\partial S_y}{\partial y} + T_d$$
<sup>(21)</sup>

where  $\varepsilon_{por}$  is the bed porosity,  $z_b$  is the bed elevation (m),  $S_x$ ,  $S_y$  are the total sediment transport components per unit width in the x- and y-directions (m<sup>2</sup> s<sup>-1</sup>), and  $T_d$  is the deposition or erosion rate of suspended sediment (m s<sup>-1</sup>).

### 384 Experimental Design

385 Twelve deltas were simulated prograding into isothermal, freshwater basins of varying initial water 386 depths that experienced varying rates of base level fall (Fig. 4). Basin depths were set to 4, 8, 12, and 20 m deep and at each basin depth the rates of base level fall varied among 0, 5, and 10 mm vr<sup>-1</sup>. Delta 387 388 growth was terminated when the ratios of initial basin volume to the volume of sediment that had 389 entered the basin were identical. For example, the deltas were allowed to prograde into the 8 m deep 390 basin for twice as long, and therefore received twice the sediment as in the 4 m deep basin. Base level 391 fall was simulated by prescribing a constant rate of decrease in water level at the open boundaries of the model. The trunk stream discharged 1000  $\text{m}^3\text{s}^{-1}$  of water into the basin along with 450 kg s<sup>-1</sup> of 392 393 sediment. This sediment load is roughly 8 times larger than that of the Goose River, but equal in size to 394 many medium-size river systems. The higher sediment load was necessary to complete the simulations 395 in a computable time. Five size fractions were weighted to form an approximate lognormal distribution around a  $D_{50}$  of 170 µm (45 kg s<sup>-1</sup> of 25 µm, 112.5 kg s<sup>-1</sup> of 50 µm, 135 kg s<sup>-1</sup> of 150 µm, 112.5 kg s<sup>-1</sup> of 396  $250 \,\mu\text{m}$ ,  $45 \,\text{kg s}^{-1}$  of  $275 \,\mu\text{m}$ ). We make the assumption that bankfull discharge is required to effect 397 398 morphologic change. In nature, bankfull discharge is limited to a small fraction of the year. We used a 399 14-day intermittency factor in the simulations in which 14 days of simulated bankfull discharge and

400 subsequent morphologic change in Delft3D is equal to the amount of bankfull discharge expected in one

401 year. In addition, each hydrologic timestep was made to equal 500 morphologic timesteps by letting



402  $f_{MORPHFAC}$  in Eqn. 18 equal to 500.

403

404 **Figure 6.** Schematic of the model domain.

405 The computational domain (Fig. 6) consisted of an open basin 15,750 m wide and 9,000 m long,

along the southern edge of which sat a 1000 m wide coast of constant 3 m elevation. The beach face

407 was 500 m wide and sloped seaward to the ultimate basin depth of a given run. Through the beach at a

408 point equidistant from the western, northern, and eastern open boundaries flowed a trunk stream 150 m

409 wide and 1300 m long with an initial depth sloping linearly from 4 m deep at the boundary to the

410 ultimate basin depth of a given simulation. The western, northern, and eastern edges of the 411 computational domain were open boundaries through which water and sediment could be transported 412 freely. The basin was free of waves, tides, and Coriolis acceleration. The fluid density of the basin, 1000 kg m<sup>-3</sup>, is constant and equal to that of the river. Near the river mouth the state variables were 413 414 computed on a 25 by 25 m square grid; in the outer region the spacing was increased to 100 x 100 m. 415 This allowed for the region of interest to be far from the boundaries without sacrificing too much 416 computational time. To meet the Courant-Friedrichs-Lewy condition for stability and accuracy the time step was set to 6 s. All Delft3D input files to reproduce the simulated delta experiencing 10 mm vr<sup>-1</sup> of 417 418 BLF in a 4 m deep basin are included in Appendix A.

419

422

## 420 Model Results

## 421 *Delta Planform Morphology*

423 The deltas predicted by Delft3D for basins of varying initial depth and rates of relative base level fall are 424 illustrated in Figure 5. The deltas are compared at the time when the ratios of basin accommodation 425 space to cumulative volume of sediment delivered to the basin are all equal. Thus the delta formed in a 426 20 m deep basin with no BLF is composed of five times the volume of sediment as the 4 m basin and 427 has taken five times as long to form. Inspection of Figure 7 shows that deltas prograding into shallower 428 basins experiencing little or no relative base level fall possess rectangular shore-parallel planforms of 429 low rugosity, compared to deeper water, falling base level deltas which are narrower and more birdsfoot 430 in planform. The latter develop more rugose shorelines and down-stepping abandoned lobes. Also, they 431 are more likely to have fewer simultaneously active distributary channels and these channels are more 432 likely to migrate laterally, forming inset strath terraces underlain by abandoned channel fill.



**Figure 7.** Bed elevation of the simulated deltas. A diagonal line from upper left to lower right represents an increase in initial accommodation space and an increase in the rate at which that accommodation is lost through time. Shoreline trajectories become steeper along this diagonal line.
435

436 A diagonal line from upper left to lower right in Figure 7 represents an increase in initial 437 accommodation space and an increase in the rate at which that accommodation is lost through time. For 438 a fixed sediment feed, as in these experiments, a deeper initial basin creates a slower rate of delta-front 439 progradation. Higher rates of BLF decrease the elevation of the shoreline at a faster rate. The 440 combination of these two vectors defines the trajectory of the delta shoreline. We measure this as a 441 slope,  $S_T$ , as defined by Eqn. 1 (Fig. 8). Shoreline trajectory can therefore provide information about initial basin depth and rate of BLF when  $S_T < 0$ . This is advantageous because the shoreline trajectory is 442 443 measurable in seismic lines and field outcrops (Posamentier and Morris, 2000). Thus if one measures 444 shoreline trajectory and gains some insight into the rate of BLF and basin depth a delta was forming in, 445 then he/she can predict the morphologies and internal geometries for that delta.



Shoreline Trajectories

447 Figure 8. Shoreline trajectories produced from the Delft3D simulated deltas shown in Figure 7 448 experiencing base level fall. They were measured through time using Equation 1. Each run with base 449 level fall is shown here labeled with the initial basin depth, the rate of base level fall, and time-averaged 450 S<sub>T</sub>.

451 The contributions of each variable—initial basin depth and rate of BLF—can be understood by holding one constant while varying the other. The R<sup>2</sup> values are coefficients of determination from linear 452 453 regressions of the logarithmic-transformed data are used to make power law relationships linear. They 454 describe what percentage of the variability in the dependent variables (y-axis) can be accounted for by 455 the independent variables (x-axis). F-tests run on the simple linear regressions yield the statistical 456 significance of the relationship (p-values). P-values less than 0.05 represent greater than 95% and are 457 considered to be statistically significant. Ignoring rate of BLF and treating each simulated delta as an 458 independent realization, reveals that increasing initial basin depth decreases the time-averaged number of active distributaries ( $R^2 = 0.85$ ,  $p = 1.7 \times 10^{-5}$ ) (Fig. 9), increases the avulsion period ( $R^2 = 0.86$ , p =459 1.4 x 10<sup>-5</sup>) (Fig. 10), creates significantly more rugose shorelines ( $R^2 = 0.62$ ,  $p = 2.4 \times 10^{-3}$ ) (Fig. 11), 460 the area of individual delta lobes decreases ( $R^2 = 0.43$ , p = 0.02) (Fig. 12), decreases topset/foreset ratios 461  $(R^2 = 0.53, p = 0.0196)$  (Fig.13), and increases average clinoform dip magnitudes ( $R^2 = 0.91, p = 1.6 x$ 462  $10^{-6}$ ) (Fig. 14), and foreset dip azimuths become more variable ( $R^2 = 0.73$ ,  $p = 3.68 \times 10^{-4}$ ) (Fig.15). 463 464 Initial basin depth has little effect on delta topset roughness, overall topset area, and delta aspect ratio. If 465 initial basin depth is held constant while BLF rate increases, the model results predict that topset roughness increases ( $R^2 = 0.85$ ,  $p = 1.9 \times 10^{-5}$ ) (Fig. 16), total delta topset area increases ( $R^2 = 0.83$ , p =466 4.1 x 10<sup>-5</sup>) (Fig. 17), and the aspect ratio decreases indicating more elongate deltas ( $R^2 = 0.39$ , p= 0.029) 467 468 (Fig. 18). There is no aggradation of the topset outside of distributary channels when there BLF.



**Figure 9.** The time-averaged number of active distributaries decreases significantly according to a power law relationship with basin depth ( $p = 1.7 \times 10^{-5}$ ).





- $(p = 1.4 \times 10^{-5}).$





**Figure 11.** Shoreline rugosity increases significantly with basin depth in a linear relationship 479  $(p = 2.4 \times 10^{-3}).$ 



**Figure 12.** The average delta lobe area shows a moderate correlation with basin depth. The linear relationship is statistically significant (p = 0.02).







**Figure 14.** The average clinoform dip magnitude shows a strong linear correlation with basin depth

488 (p=  $1.74 \times 10^{-6}$ ).



**Figure 15.** Foreset dip azimuths become more variable (lower values of  $\overline{R}$ ) as basin depth increases (p=3.68 x 10<sup>-4</sup>).



**Figure 16.** Topset roughness exhibits a strong linear relationship with the rate of BLF ( $p = 1.85 \times 10^{-5}$ ).



497 **Figure 17.** The total area of the delta topset increases linearly with the rate of BLF ( $p = 4.06 \times 10^{-5}$ ).



**Figure 18.** Aspect ratios decrease as rates of BLF increase indicating that deltas become more elongate under BLF forcing (p=0.029).

504

#### 503 Delta Internal Geometry

505 Of particular interest are the accretionary deposits that form in distributary channels. They form as 506 discrete packages of sediment separated by chronostratigraphic, accretionary surfaces. These 507 accretionary deposits are seen in all simulated deltas regardless of BLF or initial basin depth (Fig. 19). 508 The distance between two accretionary surfaces along an axis perpendicular to the channel's centerline 509 decreases as initial basin depth increases, indicating a slower rate of accretion for the deposit. Under 510 high rates of BLF, down-stepping terraces form (Fig. 20). Inspection of bed elevations through time 511 show that these terraces arise as the distributary channels migrate laterally within the incised distributary 512 channel. Consequently, there is a trajectory for these accretionary surfaces that is analogous to the 513 shoreline trajectory because it becomes steeper with deeper initial basin depths and higher rates of BLF. 514 (Note: More Delft3D simulated internal geometry can be seen in Appendix C).

515 BLF and basin depth do not exhibit a strong effect on the spatial grain size distributions of 516 simulated deltas. The coarsest grains are located in the topset and upper foreset. Mud drapes occur 517 intermittently in both distributary channel fills and clinoforms. The lower foreset tends to be finer-518 grained. All deltas, regardless of initial basin depth or rate of BLF, exhibit weak lobe fining from 519 proximal to distal, although this trend is not statistically different from no trend. As a result, we must 520 consider mean delta lobe grain size to remain statistically constant from proximal to distal.

521 Clinoform heights and mean dip magnitudes decrease from proximal to distal with BLF. 522 Clinoform heights, measured from the rollover point to the basin floor, decrease systematically as base 523 level falls. The trajectory of the clinoform rollover defines the shoreline trajectory. No subaqueous 524 clinoform rollovers formed in any of the simulated deltas thus precluding the existence of 'fore-525 shortened' stratigraphy in the model (Posamentier and Morris, 2000). As base level falls, the delta is 526 prograding in to shallower water which results in decreasing clinoform dip magnitudes from proximal to

- 527 distal. Clinoform dip magnitudes also decrease in the absence of BLF because the delta is prograding on
- 528 top of previously deposited pro-delta muds which cause a reduction in water depth. Steepening
- 529 clinoform dip magnitudes are not observed in any of the simulated deltas.







Figure 20. Model results shown are from a simulated delta prograding into 20 m water depth and experiencing 10 mm yr<sup>-1</sup> BLF ( $S_T = -0.02$ ). Inset strath terraces forms regardless of rate of BLF. The down-stepping of the inset terraces is a result of the accretion rate and the rate of BLF, and can be thought of as analogous to shoreline trajectory.

#### 532 **Discussion**

- 533 Shoreline trajectory is set by the rate of BLF and the progradation rate of the delta, and the latter is set
- by basin depth and BLF. By considering the effect of  $S_{T}$ , we are essentially weighting the relative
- importance of rate of BLF and basin depth on the formation of a delta. To illustrate the relationship
- between the rate of BLF, basin depth, and shoreline trajectory we propose a 2D model of delta
- 537 progradation. It can be extended to account for radial growth of a delta, but this effect is excluded here

538 for simplicity.

#### 539 2D Model Derivation

- 540 Using a material balance law we assume that the amount of sediment fed to the delta front,  $q_s$  (m<sup>2</sup>
- 541 s<sup>-1</sup>), must fill the accommodation space to base level, or:

$$q_s = H \frac{dx}{dt} \tag{22}$$

- 542 where H (m) is the water depth at time, t (seconds), x is the position of the shoreline (m), and  $\frac{\partial x}{\partial t}$  is 543 the rate of progradation (m s<sup>-1</sup>). H varies with time in proportion to the rate of BLF,  $\dot{r}$  (m s<sup>-1</sup>). This
- 544 relationship can be defined for a constant rate of BLF as,

$$H = H_0 - \dot{rt} \tag{23}$$

545 where  $H_0$  is the initial basin depth (m). Therefore Eqn. 21 becomes,

$$q_s = (H_0 - \dot{r}t)\frac{dx}{dt} \tag{24}$$

To account for possible incision of the topset, we consider that the sediment flux delivered to the shoreline varies as a function of the sediment flux of the trunk stream,  $q_{so}$  (m<sup>2</sup> s<sup>-1</sup>), the rate of BLF, and position of the shoreline such that,

$$q_s = q_{so} + \dot{r}x \tag{25}$$

549 A scenario could arise in which all of the previously deposited material down to the new base level

550 is re-excavated during BLF, thus requiring a steepening of slope. We, however, ignore changes in

551 bed slope. Substituting Eqn. 24 into Eqn. 23:

$$q_{so} + \dot{r}x = (H_0 - \dot{r}t)\frac{dx}{dt}$$
<sup>(26)</sup>

552 which can be rearranged as,

$$\frac{dx}{q_{s0} + \dot{r}x} = \frac{dt}{H_0 - \dot{r}t} \tag{27}$$

553 Each side is of the form ,

$$\int \frac{dx}{a+bx} = \frac{1}{b} \ln(a+bx)$$
<sup>(28)</sup>

554 Therefore we can integrate the ordinary differential equation to get,

$$\frac{1}{\dot{r}}\ln(q_{s0} + \dot{r}x)\Big|_{0}^{x} = -\frac{1}{\dot{r}}\ln(H_{0} - \dot{r}t)\Big|_{0}^{t}$$
(29)

555 which can be rewritten as,

$$\ln(q_{s0} + \dot{r}x) - \ln(q_{s0}) = -[\ln(H_0 - \dot{r}t) - \ln(H_0)]$$
(30)

556 or,

$$\ln\left(\frac{q_{s0} - \dot{rx}}{q_{s0}}\right) = -\ln\left(\frac{H_0 - \dot{rt}}{H_0}\right) \tag{31}$$

557 This can be further simplified to,

$$\frac{q_{s0} - \dot{rx}}{q_{s0}} = \frac{H_0}{H_0 - \dot{rt}}$$
(32)

558 Solving for x yields,

$$x = \frac{q_{s0}}{\dot{r}} - \frac{q_{s0}H_0}{\dot{r}(H_0 - \dot{r}t)}$$
(33)

Taking the derivative of x yields the rate of horizontal progradation,  $\frac{dx}{dt}$  (m s<sup>-1</sup>),

$$\frac{dx}{dt} = \frac{q_{s0}H_0}{(H_0 - \dot{r}t)^2}$$
(34)

Therefore the horizontal progradation rate is proportional to both the sediment flux,  $q_{s0}$ , and  $\frac{H_0}{(H_0 - \dot{r}t)^2}$ . The latter is a scaled ratio such that at t=0, and for very large H<sub>0</sub> the term is approximately  $\frac{1}{H_0}$  and the rate of progradation is essentially independent of  $\dot{r}$ . For t approaching  $\frac{H_0}{\dot{r}}$ , the term becomes infinitely large as base level approaches the basin floor. In this case the rate of BLF sets the progradation rate. Thus for constant  $q_{s0}$ ,  $H_0$  sets the scale, while the rate of BLF, sets the progradation rate. Furthermore the shoreline trajectory can be defined as,

$$S_{T} = -\arctan\left(\frac{H_{0} - \dot{r}t}{\frac{q_{s0}}{\dot{r}} - \frac{q_{s0}H_{0}}{\dot{r}(H_{0} - \dot{r}t)}}\right)$$
(35)

This case is strictly 2D which may be appropriate for the simulated deltas that incise their topset, and become elongate, thereby inhibiting radial growth.

568 Analysis

569

570 As the above analysis indicates, both basin depth and the rate or BLF control S<sub>T</sub> but one dominates the 571 other under selected conditions. The relative influence of basin depth and rate of BLF on each variable 572 can be gleaned from a multiple linear regression (MLR) of the variable as a function of basin depth and 573 rate of BLF. P-values associated with F-tests assess the fit of the MLR to the data; p-values less than 574 0.05 provide greater than 95% confidence that the model possesses a statistically good fit. Student's t-575 tests of MLR correlation coefficients yield p-values indicating the individual statistical significance of 576 basin depth and rate of BLF. Basin depth and rate of BLF are deemed statistically significant if their 577 respective t-test p-values are less than 0.05 (greater than 95% confidence).

Examination of the MLR results in Table 1 indicates that basin depth plays a stronger role than rate of BLF in setting the number of active distributaries, shoreline rugosity, average area of delta lobes, and avulsion period. Conversely, rate of BLF influences topset roughness, total area of the delta topset, foreset dip azimuth statistic, and the coefficient of determination for progressive lobe fining more than basin depth.

583

Variable Name	F-test p- value	Basin Depth <i>t-</i> test <i>p-</i> value	Rates of BLF <i>t-</i> value <i>p-</i> value	Stronger Predictor
Number of Active				
Distributaries	2.67E-03	8.50E-04	0.46	Depth
Avulsion Period	1.38E-04	3.81E-05	0.81	Depth
Shoreline Rugosity	2.63E-03	1.34E-03	0.083	Depth
Average Delta Lobe Area	0.012	0.01042	0.060	Depth
Foreset Dip Azimuth				
Variance	4.15E-03	7.88E-04	0.17	Depth
Aspect Ratio	0.038	0.17	0.024	BLF
Topset Roughness	1.68E-04	0.69	1.68E-04	BLF
Total Delta Area	8.87E-05	0.10	3.01E-05	BLF

**Table 1.** The results from the multiple linear regression (MLR) indicate how strongly basin depth and rate of BLF influence each variable. F-tests determine the quality of the MLR model fit to the data. The p-values associated with the F-tests indicate the statistical confidence we have that the MLR model is a good fit. Student's t-test assess the relative contribution of basin depth and rate of BLF to the MLR model. The resulting p-values indicate whether basin depth or rate of BLF are a strong predictor for each variable. P-values less than 0.05 are considered statistically significant.

590

591 Shoreline rugosity correlates with basin depth and steeper shoreline trajectories because basin

592 depth reduces the number of active distributaries and increases the avulsion period. There are fewer

active distributaries in deeper basins because it takes a longer period of time for river mouth bars to

- aggrade to a bed elevation at which they can bifurcate distributaries, therefore deeper basins have fewer
- 595 bifurcations and thus fewer active distributary channels. Fewer active distributaries create a less
- equitable distribution of sediment around the delta's perimeter. Avulsions occur when the distributaries

597 aggrade and test their levees in order to attain a steeper water surface slope (Slingerland and Smith 598 2004). Distributaries forming in deeper basins require more time to aggrade to the bed elevation where 599 they can test their levees, therefore, avulsion period increases with deeper initial basin depths. Less 600 frequent changes in the position of active distributaries due to longer avulsion periods, focuses 601 deposition around the perimeter to only a few locations for a long time. Fewer active distributaries and 602 longer avulsion periods result less equitable distribution of sediment to around the delta's perimeter 603 which in turn causes highly rugose shorelines (Figs. 21 and 22) and highly variable foreset dip azimuths. 604 MLR results show that shoreline rugosity is effected by rate of BLF as well as basin depth, likely 605 through BLF inhibiting mouth bar formation and channel bifurcation, therefore it may also be 606 appropriate to conceptualize shoreline rugosity as a function of shoreline trajectory when  $S_T < 0$ . 607 Shoreline rugosity can be predicted using the following MLR equation:

608

$$\log Shoreline Rugosity = 0.32 * \log Basin Depth - 0.2 * \log Rate of BLF$$
(35)



610 611 **Figure 21.** Shoreline rugosity decreases significantly as the number of active distributaries increases (p 612  $= 2.1 \times 10^{-4}$ ). High numbers of active distributaries are able to deliver sediment to the shoreline more 613 equitably resulting in fan deltas with smooth shorelines.



**Figure 22.** Shoreline rugosity increases as the avulsion period ( $p=3.78 \times 10^{-3}$ ). Long avulsion periods

focus sediment deposition at one locality for a longer period of time, thereby causing irregularly-shaped,rugose shorelines.

619 The shoreline trajectory is a good predictor of a delta's internal geometry and vice versa. As the 620 shoreline trajectory steepens, clinoform heights decrease from proximal to distal. Accurate clinoform 621 heights may be difficult to measure in the rock record though, due to subsequent erosion. Clinoform dip magnitudes, on the other hand, have a high preservation potential and could provide a useful metric for 622 623 identifying basin depth and BLF in ancient deltas. The average clinoform dip magnitude is strongly 624 dependent upon the basin depth (Fig. 13) because deeper basin depths result in tractional sediment 625 transport occurring over a smaller portion of the delta front than in shallower basins. Tractional 626 sediment transport creates shallower clinoform slopes than suspended transport, therefore we expect 627 deeper initial basin depths to result in tractional transport accounting for less of the total sediment 628 transport along the delta front and thus larger clinoform dip magnitudes. Clinoform dip magnitudes 629 decrease from proximal to distal under BLF if the basin floor bathymetry is flat because of the delta is 630 prograding into increasingly shallow water. It should be noted, however, that Delft3D lacks an 631 algorithm to account for slumps or other gravity-driven flows of sediment down the delta foreset, 632 thereby overestimating clinoform dip magnitudes. The effects of clinoform height and dip magnitude 633 can be conceptualized for deltas of varying shoreline trajectories prograding into basins with varying 634 slopes. In Figure 23 it can be seen that when the shoreline trajectory is steeper than the basin slope, 635 which is the case in the simulated deltas, that BLF results in shorter clinoform heights and shallower 636 clinoform dips magnitudes. When the shoreline trajectory and basin slope are equal clinoform heights 637 and dip magnitudes should remain constant. In the scenario where the shoreline trajectory is shallower 638 (or zero) than the basin slope, increasing clinoform heights and dip magnitudes should increase. Note 639 that BLF is not a necessary condition for increased clinoform dip magnitudes.



Figure 23. Conceptual diagram of clinoform height and dip varying based upon relationship between shoreline trajectory and basin slope. When  $S_T >$  basin slope, clinoform heights and dip magnitudes decrease from proximal to distal. When  $S_T$  =basin slope, clinoform heights and dip magnitudes remain constant. When  $S_T <$  basin slope, or  $S_T$ =0, clinoform heights and dip magnitudes increase from proximal to distal.

646 Foreset facies increase in thickness more with increasing basin depth than their corresponding 647 topset because the topset thickness is set by the relatively constant height of levees and point bars in 648 distributary channels. This in turn causes topset/foreset ratios to decrease with increasing basin depth. 649 The statistically constant average grain size of delta lobes from proximal to distal indicates that neither 650 basin depth nor rate of BLF have any significant impact on grain size. This stands in contrast to the 651 predictions made by Posamentier and Morris (2000), but it must be noted that the modelling presented 652 here does not account for rejuvenation of the fluvial catchment which could feasibly cause an increase in 653 average grain size over time.

654 In summary, basin depth and rate of BLF are good predictors of a simulated delta's planform and 655 internal geometry. If all other factors except basin depth and rate of BLF are held constant, increasing 656 basin depth decreases the number of active distributaries, increases shoreline rugosity, decreases average 657 area of delta lobes, increases avulsion period, and increases foreset azimuth dip variance. Increasing 658 rates of BLF lead to greater topset roughness, a larger total area of the delta topset, and a more elongate 659 aspect ratio. Shoreline trajectory, for cases where there is BLF and  $S_T < 0$ , may better predict the effects 660 of initial basin depth and BLF on the number of active distributaries and the shoreline rugsoity than 661 either basin depth or BLF could alone. Physical processes including greater time periods required for 662 aggradation within distributary channels can be linked to a deeper basin depths and lead to longer 663 avulsion periods and fewer active distributaries. Consequently, deposition is focused in one or two 664 locations for a long time before the locus of deposition shifts, thereby causing highly rugose shorelines 665 and complex delta front geometries.



**Figure 24.** The Goose River Delta is located in Goose Bay, Labrador, Canada (A) where is prograding into the tip of the Lake Melville fjord (B). (C) is located at the X marked in (B).

#### 670 Testing Model Predictions

#### 671 Goose River Delta

# To test the predictions of the Delft3D modelling we compare the model results to morphological and

#### 673 stratigraphic data collected from the Goose River Delta located in Goose Bay, Labrador, Canada. Here

#### 674 the Goose River drains a 3436 km<sup>2</sup> catchment (Anonymous, 2001) into the western tip of Lake Melville

#### 675 (Fig. 24). The Goose River Delta was chosen for this study because post-glacial rebound in the region

#### has resulted in 5 mm yr<sup>-1</sup> of BLF over the last 8,000 years (Clark and Fitzhugh 1992; Liverman 1997).

#### 677 Radiocarbon and OSL dates in combination with the elevation of abandoned delta lobes corroborate a

### BLF rate of 5 mm yr<sup>-1</sup>. The delta consists of two active lobes with at least three inactive lobes upstream.

#### The river is ungauged; sporadic measurements taken from 1948 to 1952 (Coachman, 1953) indicate

highly variable discharges ranging from 5 m<sup>3</sup> s<sup>-1</sup> in March to 532 m<sup>3</sup> s<sup>-1</sup> during the spring freshet in May.

681 The sediment load of the Goose River is unknown. Laser particle size analysis of sediment samples 682 collected from topset and foreset facies, including bottom grabs from the modern delta front, were 683 weighted by measuring the vertical distance between samples and interpolating to approximate the change in grain size moving down the delta front. Interpolated values were then averaged to obtain an 684 685 average grain size in the Goose River Delta of 150 µm, with grains ranging from ~10 cm diameter 686 cobbles to  $< 20 \mu m$  clays. The Goose River Delta probably prograded over an irregular fjord bathymetry; at present it is prograding into 30 m water depth. The shoreline trajectory of the Goose 687 688 River Delta over the last 5350 years was estimated by calculating the slope of a straight line from a large 689 distibutary (perhaps the paleo-trunk stream) identified in the upper-most abandoned lobe to the present day shoreline of the southern active lobe. It is  $-0.15^{\circ}$  (S<sub>T</sub> =  $-2.6 \times 10^{-3}$ ). Given the Goose River Delta's 690 691 average grain size and relatively shallow shoreline trajectory, its morphometry should be most closely predicted by the simulated delta which prograded into 20 m water depth under a 5 mm yr<sup>-1</sup> BLF forcing. 692



**Figure 25.** Locations of the stratigraphic sections indicated on a digital elevation map of the Goose

- River Delta. Delta lobes are outlined in black corresponding to the yellow outline, P, enclosing the area, A, in Figure 2. Darker colors represent higher elevations while lighter colors are lower elevations. The
- 697 contours are elevations with a contour interval of 2 m.



698 699 Figure 26. Locations of GPR lines collected along the southern active lobe of the Goose River Delta are 700 indicated here in black.

#### 702 Methods

- 703 Stratigraphic sections were logged at four locations (Figs. 27-31, see Fig. 25 for locations) in the Goose
- 704 River's cut banks where sediments of abandoned delta lobes are exposed. The section at locality 3
- 705 (Location 3, Fig. 25) was extended downward by sinking a 3.6 m vibracore from 0.5 m above river
- 706 level. Ground penetrating radar data were collected along the lines shown in Figure 26 with a Software

707 and Sensors pulseEKKO PRO GPR using 100 MHz antennae. GPR data were processed by dewowing 708 the data, applying a bandpass filter, and migrating the data using an F-K Stolt migration with a 1-layered velocity model with halfspace velocity of  $0.6 \text{m ns}^{-1}$ .  $0.6 \text{m ns}^{-1}$  is the velocity of electromagnetic waves 709 710 through water-saturated clay and sand. The GPR data were then converted from the time to depth 711 domain. Clinoforms were identified in the lines and their slope was measured using a linear line fitted 712 using MATLAB. Rapid attenuation of high frequency energy resulted in poor data quality with spurious 713 low frequency signals at depth. As a result, only lines with clear clinoforms were retained for use in the 714 dataset. (Processed and interpreted GPR lines can be examined in Appendix D).

715 The morphometry of the Goose River Delta was defined from an aerial photo, single beam and 716 multibeam bathymetric data, parabolic echosounder data, and dGPS measurements. A composite aerial 717 photo was taken from a helicopter in August 2012. At the time, the tide and flow discharge were low 718 providing maximum subaerial exposure. Bathymetry data were collected using a single-beam fish finder 719 as well as a RESON 7125SV2 200/400kHz multibeam echo sounder (MBES). The MBES was used in 720 conjunction with an Applanix POS-MV motion reference unit to correct for movement of the boat. This 721 combination allowed for bed elevations to be mapped accurately to within 0.05 m. We defined the 722 shoreline as the -1m contour because that is the shallowest reliable depth from the MBES. The sub-723 bottom stratigraphy was imaged using an Innomar Parametric Echo Sounder (PES) operating at 6 kHz 724 and 100kHz. Real-time kinematic GPS was used to provide horizontal positional accuracy of 0.02 m.



Figure 27. Stratigraphic section from location 1 in Fig.28. (N 53.39694°, W 60.40011°)
(Slingerland,2013).



**Figure 28.** Stratigraphic section from location 2 in Fig.28 (N 53.3874139°, W 60.38614°)









735 736 Figure 30. Graphic log of vibracore sunk 0.5m above river level at location 3 in Fig. 28. (N 53.38744°, W 6038478°). Depositional dips of beds are not shown due to uncertainty in dip magnitudes. 737



- - **Figure 31.** Stratigraphic section from location 4 in Fig.28. (N 53.38733°, W 60.38397°).

741 **Results** 

The Goose River Delta's shoreline trajectory is  $-0.15^{\circ}$  (S<sub>T</sub> =  $-2.6 \times 10^{-3}$ ). Combined, the northern and 742 743 southern active lobes of the Goose River Delta possess four to five (mean =4.333) distributaries time-744 averaged from 1952 to 2012 with a maximum width of at least 50 m (Fig. 32). Five delta lobes created 745 via lobe switching events (avulsions) over the last 5350 years were identified by careful study of the 746 digital elevation model (DEM). (Fig. 25 and 33), Thus the avulsion period is 1070 years. The Goose 747 River receives only an eighth of the sediment of the simulated deltas, therefore the scaled avulsion 748 period is  $1070 \div 8 = 134$  years. A rough estimation of the sediment flux was made to normalize the 749 avulsion period by estimating the volume of sediment in the Goose River Delta and dividing that by the 750 oldest measured radiocarbon date (5350 years). We assumed the previous bathymetry sloped from 751 roughly 15 m water depth to the present day 30 m water depth in order to make this sediment flux 752 estimate. Multibeam bathymetry data indicate a mean clinoform dip magnitude of 4° with a standard 753 deviation of 4.4°. Similarly, GPR data indicate a mean clinoform dip magnitude of 3.9° with a standard 754 deviation of 2.5°. The modern clinoform (foreset) is steepest at the top with dips averaging between 10-755 12°, decreasing to horizontal at the base. Interpretation of the DEM and orthophotos yield a shoreline 756 rugosity of 2.3 for the Goose River Delta complex (including the abandoned lobes). dGPS points along a 757 random strike line estimate the Goose River Delta's topset roughness to be 0.11 m.

## Serial Orthophotos of the Goose River Delta



1987

760

Figure 32. Serial orthophotos of the Goose River Delta used to measure the time-averaged number of
active distributaries through time. Red boxes indicate the area in which distributaries were counted. We
identified five active distributaries greater than 50 m wide in 1951, five in 1970, 7 in 1975, three in
1987, three in 1998, and three in 2012. Each orthophoto was given equal weight in the average.
(Images from 1951 – 1998 from Newfoundland and Labrador Department of Conservation; 2012

765 (Images from 1951 – 1998 from NewToundiand and Labrador Department of Co.

satellite image was purchased from MapMart).

<sup>1998</sup> 

<sup>2012</sup> 





#### 770 Discussion

767

The simulated deltas can be used to predict the morphology and internal geometry of the Goose River
Delta. It is important to recognize that while grain size and shoreline trajectories may be similar in the
simulated deltas and the Goose River Delta, there are differences in basin depth, water discharge, and

- sediment discharge between the simulated deltas and the Goose River Delta. Recognizing these
- differences and testing the model against the Goose River Delta allows us to determine how applicable
- the model is to deltas with different boundary and initial conditions.
- 777 The regression equations derived from the Delft3D modeling predict one to two active
- distributaries on average for a delta with a similar basin depth to the Goose River Delta. Six aerial
- photos taken at random ice-free times document an average of four to five distributaries, fairly similar to
- the predicted, even though the serial orthophotos cover a short interval in relation to the age of the delta
- 781 (~5350 years). The disparity that exists is likely due to the fact that we are comparing simulated deltas

782 forming in flat basins to a delta forming in a ford with irregular pre-existing bathymetry. The predicted 783 avulsion period based upon basin depth for a delta like the Goose River Delta is 75 years. The observed, 784 flux-corrected avulsion period is 134 years. One possible explanation for this disparity is that the Goose 785 River Delta's sediment flux may be less than our estimate. A second explanation may be that the 786 irregular, and possibly confining, ford bathymetry limited the possibility of a steeper water surface 787 slope being through avulsions and lateral lobe switching thereby increasing the avulsion period. The 788 predicted clinoform dip magnitude for a delta with basin depth like the Goose River Delta is 1.1°. It is 789 important to note that the largest simulated clinoform dips ( $\sim 0.9^{\circ}$ ) are observed in the 20m deep basin, 790 while the Goose River Delta is prograding into 30 m water depth which is deeper than any simulated 791 delta. Goose River Delta clinoform dips are steeper than expected (4°). This disparity may reflect the 792 role of slumping (Fig.34) and other gravity driven grain flows on the delta front which is not accounted 793 for in the Delft3D simulations. Using MLR Equation 35, we predict that the shoreline rugosity for a 794 delta with a shoreline trajectory like the Goose River Delta should be five to six while the actual value is 795 two to three. Wave and tide energy acting upon the Goose River Delta may be the cause of the 796 smoother than expected shoreline. The less rugose shoreline is consistent, however, with the Goose 797 River Delta possessing more active distributaries that deliver sediment to the perimeter of the delta more 798 evenly.



799

Figure 34. Slumping down the delta front can be seen in this image produced from Parabolic Echo
Sounder data (J. Best pers. com., 2012). It is important to note that Delft3D does not account for
slumping.

#### 804 Application to the Ancient

805

806 The Panther Tongue Member of the Starr Point Formation near Helper, Utah is reported to be a forced-

807 regressive delta, but there is some level of doubt in the evidence to support this interpretation. Here we

- apply the relationships predicted by the Delft3D modeling to test the idea that the Panther Tongue Delta
- 809 experienced BLF.
- 810

#### 811 **Panther Tongue Delta**

812

813 The Panther Tongue Member of the Starr Point Formation was deposited during the Late Cretaceous 814 (Campanian; 83.6-72.1 Ma) as a deltaic succession prograding north-northeast to south-southwest into 815 the Western Interior Cretaceous Seaway (Newman and Chan, 1991; Hwang and Heller, 2002; Edwards 816 et al., 2005; Olariu and Bhattacharya, 2005; Howell, Skorstad et al., 2008, Howell, Vassel et al., 2008; 817 Enge, Howell et al., 2010a; Enge, Howell et al., 2010b; Enge, Howell et al., 2010c; Hampson, Gani et 818 al., 2011) (Fig. 35 and Fig. 36). The Panther Tongue Mbr. was first described as a deltaic "parasequence" 819 deposited at eustatic lowstand" (Newman and Chan 1991), and later re-characterized as a falling stage 820 systems tract (FSST) (Posamentier, Morris et al. 1995). As evidence that the Panther Tongue was 821 deposited during a fall in relative sea level, Posamentier and Morris (2000) cited: 1) a basinward 822 decreasing clinoform height, due to a shallowing of water depth; 2) an absence of preserved delta topset 823 deposits; 3) a sharp-based contact between the FSST and the underlying highstand systems tract (HST), 824 in this case the Mancos Shale; 4) a shift from proximal, inertia-dominated suspension-type deposition to 825 distal bed-load dominated deposition; and, 5) fore-shortened stratigraphy, where clinoform heights are 826 less than would be expected for a given water depth (i.e., a 20 m high clinoform forming in 75 m of 827 water). In a later paper, Posamentier and Morris (2000) cited the Panther Tongue as an example of a 828 classic forced regressive delta, even though their criterion 1 cannot be applied to the PT because of poor 829 outcrops and subsequent ravinement at the beginning of the transgressive systems tract. Criterion 5 830 cannot reasonably be used as evidence of a forced-regressive origin for the Panther Tongue Mbr. 831 because subaquoeous clinoform rollovers can exist even in deltas experiencing relative base level rise 832 like the Fly River Delta of Papua New Guinea (Slingerland et al., 2008). They acknowledged that each 833 of their lines of evidence alone was circumstantial, but proposed that when observed together the 834 converging lines of evidence strongly indicated a forced regression. Hwang and Heller (2002), make a
significant contribution by recognizing what they called lowstand, healing phase deposits onlapping
clinoforms of the Panther Tongue Mbr. on the east side of Price River Canyon. Furthermore, they
recognized the ravinement surface at the top of the Panther Tongue as a transgressive lag deposit, further
corroborating the notion that the Panther Tongue belongs to the FSST.

839 The shoreline trajectory of the Panther Tongue Mbr. is debated. Howell, Skorstad, et al. (2008) 840 assigned the Panther Tongue a positive shoreline trajectory of 0.07 degrees which, if accurate, would be 841 inconsistent with a forced-regressive origin. In conflict with this shoreline trajectory, they also cited 842 Posamentier and Morris (2000), and stated that the Panther Tongue Delta was deposited during a forced 843 regression. We assume then, that they did not follow the convention of other workers who defined the 844 trajectory as negative downwards. Even so, it is unclear how they determined this value, because the 845 clinoform rollovers from which one would measure a shoreline trajectory have been removed by the 846 subsequent ravinement surface. Hampson, Gani et al. (2011) interpreted the Panther Tongue as a single 847 parasequence containing multiple delta lobes experiencing BLF. They ascribed a shoreline trajectory of -848 0.02° to the Panther Tongue Mbr. by using a novel approach in which they measured the down-dip 849 pinchout of proximal delta front deposits in a dip-oriented outcrop perpendicular to the subregional 850 shoreline orientation. This requires accurately removing the local tectonic dip which is large ( $\sim 7^{\circ}$ ) 851 compared to the  $S_{T}$ .

The reported rates and magnitudes of BLF for the Panther Tongue Delta vary considerably, with limited evidence provided to support one value over another. Hampson, Gani et al. (2011) conjecture that low-amplitude (< 30m), high-frequency (< 400 kyr) glacio-eustatic, relative sea level cycles controlled the deposition of the Panther Tongue. They cited a lack of topset facies and offlapping delta lobes as evidence of BLF during Panther Tongue times. However, the authors claim there is little evidence to suggest BLF during deposition of a time-equivalent wave-dominated shoreline to the south

858 of the Panther Tongue Mbr. To reconcile this conflict, the authors proposed that the un-named wave-859 dominated shoreline to the south was deposited during a period of relative base level rise and that 860 subsequent BLF resulted in the rapid progradation of the Panther Tongue Delta. In Sowbelly Gulch, 861 near Standardville, UT, Newman and Chan (1991) observed single-story sand bodies that they 862 interpreted to be distributary channel deposits. Olariu and Bhattacharya (2005) called these channel 863 facies "terminal" distributaries, cutting river mouth bars. The bars then aggraded upstream and laterally 864 filled them. The resulting sand bodies were preserved in a delta-front environment free of subaerial 865 erosion. Both aggradational mouth bars and a lack of subaerial erosion seemingly conflict with BLF 866 occurring during deposition of this proximal area of the Panther Tongue Mbr. A contrasting 867 interpretation suggests that these channels were submarine channels formed in an estuarine environment 868 during subsequent relative base level rise (Hwang and Heller 2002).

869 The water depth into which the Panther Tongue Delta prograded has received limited attention 870 from previous researchers, and depth estimates that do exist are not well justified. Posamentier and 871 Morris (2000) cite unpublished biostratigraphical data from a personal communication, arguing that the 872 Panther Tongue Delta prograded into water depths deeper than 75 m. They use this water depth estimate 873 in relation to the typical, preserved clinoform height (~25 m) as evidence of fore-shortened stratigraphy 874 and a forced-regressive origin of the Panther Tongue Mbr. However, a more reliable estimate of paleo-875 water depth can be obtained by assuming that wave-rippled strata were deposited at or above fair 876 weather wave base (typically 5-20 m). In the proximal portions of the Panther Tongue Mbr., both 877 Newman and Chan (1991) and Olariu et al. (2010) document wave ripples in lower delta front sands 878 positioned less than 2 meters above the basal, prodelta muds. The presence of wave ripples in a lower 879 delta front depositional environment indicates that the delta was prograding into water very close to fair 880 weather wave base. Based on this reasoning and truncated clinoform heights of up to 25 m, we propose

that the Panther Tongue Delta prograded into a paleo-water depths of 20-30 m. This is similar to the 1030 m water depths conjectured for the Turonian Ferron Sandstone Mbr. in a similar tectonic setting 50
km to the south (Ahmed et al., 2014).

884 Measurements of clinoform dip magnitudes are more consistent across previous studies, although 885 limited in spatial distribution to the northern proximal portion of the Panther Tongue Mbr. near Helper, 886 UT. In a series of papers (Enge and Howell 2010a, Enge, Howell et al. 2010b, Enge, Howell et al. 2010c), the authors reported clinoform dips ranging from 0.4° to 2.65° as measured by LIDAR in the 887 888 proximal portion of the Panther Tongue. Olariu et al. (2010) use LIDAR to measure clinoform dip 889 magnitudes near the study areas of Enge and Howell's (2010a, 2010b) and Enge, Howell et al. (2010) 890 and reported values ranging from fractions of a degree to 3°. Hwang and Heller (2002) reported 891 clinoform dip magnitudes of 7° in the proximal portion of the Panther Tongue Mbr. with clinoform dip magnitudes increasing to  $> 20^{\circ}$  in the distal, southern portion of the Panther Tongue Mbr. near 892 893 Huntington Canyon. Newman and Chan (1991) also reported steep clinoform dips ranging from 15° to 894 30° in the southern portion of the Panther Tongue Mbr. We interpret the published clinoform dip 895 magnitudes of the Panther Tongue Mbr. to indicate a systematic increase in dip magnitude from north to 896 south.



Figure 35. A paleo-reconstruction of the Panther Tongue Delta (after Edwards et al. 2005). Here there
are two main delta lobes, a northern lobe prograding south east and a southern lobe prograding southsouth west. Edwards et al. (2005) depict a highly rugose shoreline for the Panther Tongue Delta.



901

Figure 36. An interpretation of the Panther Tongue Delta from Olariu et al. (2010). They also depict
 three delta lobes and show the paleo-shoreline of the Western Interior Cretaceous Seaway during the
 Campanian. Their reconstruction of the Panther Tongue Delta indicate a lobate morphology.

#### 905 Methods

906 To supplement the data collected by others we measured clinoform dips and dip directions in the Panther 907 Tongue Mbr. using a laser ranger. Data were collected from locations that had two opposing cliff faces 908 containing easily identifiable clinoform beds on either side of a canyon (Fig. 5). Points in x, y, z space 909 were shot along individual clinoform beds with the laser ranger and a trend and plunge were calculated 910 relative to true north. Shooting the same or adjacent bed on the other side of the canyon provided a 911 second trend and plunge. Using the two trends and plunges, we calculated a true dip and dip direction 912 for the clinoform tops just below the truncation surface. Depositional dips were then corrected for the 913 tectonic dip obtained from the ravinement surface at each data collection location. A structure-contour 914 map of coal measures overlying the Panther Tongue Mbr. (USGS Coal Resource Occurrence Map of the

915 Standardville Quandrangle, Carbon County, Utah) was used to corroborate the tectonic dip near Price

- 916 River Canyon. Guttercasts and flutes were also measured to determine the local paleoflow direction.
- **Results**
- Clinoform dip, dip direction, and paleoflow directions are presented in Tables 2 and 3, respectively. The average clinoform dip over all exposures is 4.4°. The variability in dip direction, measured by the foreset dip azimuth statistic is 0.19 (N = 11). The mean grain size of the Panther Tongue Mbr. increases from fine sand in the proximal, northern portion of the Panther Tongue Mbr. to medium sand in the distal, southern portion of the Panther Tongue Mbr. Hampson, Gani, et al.'s (2011) measurement of - $0.02^{\circ}$  (S<sub>T</sub> = -3.5 x 10<sup>-4</sup>) and Howell, Skorstad, et al.'s (2008) measurement of -0.07° (S<sub>T</sub> = -1.2 x 10<sup>-3</sup>) will be considered the maximum and minimum estimates of shoreline trajectory for the Panther Tongue Mbr., respectively.

Location	Dip Azimuth (°)	Dip Magnitude (°)
1	169	1.5
2	169	2.5
2	274	6
4	164	2
4	239	7
4	254	11
6	180	4
6	128	12
7	253	6
8	290	11
8	328	12

- Table 2. Clinoform dips and dip directions collected from the Panther Tongue Mbr. of the Starr Point
   Fm. Locations correspond to points in Figure 3. Note that the clinoform dip magnitudes increase to the
   south.

Location Paleocurrent Indicator		Azimuth
1	Gutter Cast	200
1	Gutter Cast	215
1	Gutter Cast	221
2	Flute	204
2	Gutter Cast	204
2	Gutter Cast	210
3	Gutter Cast	220
5	Gutter Cast	210
5	Gutter Cast	224
5	Gutter Cast	230
5	Flute	234
5	Flute	235
5	Gutter Cast	244
5	Gutter Cast	245
5	Gutter Cast	248
5	Gutter Cast	248
5	Gutter Cast	252
5	Gutter Cast	252

**Table 3.** Paleocurrent indicators documented in the Panther Tongue Mbr. of the Starr Point Fm.Locations correspond to points in Figure 3.

938 **Discussion** 

939

940 The grain size, basin depth, and shoreline trajectory of the Panther Tongue Mbr. fall within, or just 941 outside, the parameter space of the model results presented earlier. Mean grain size estimates for the 942 Panther Tongue Mbr. range from fine to medium sand. The mean grain size of the Delft3D simulations 943 is 170 µm diameter fine sand. The Panther Tongue Delta likely prograded into 20-30 m water depth. 944 Simulation basin depths range from 4 to 20 m deep. Therefore, the Panther Tongue Delta probably 945 prograded at a slower rate than the simulated deltas. Shallow shoreline trajectory estimates therefore 946 indicate a slow rate of BLF. It is difficult to compare discharges (Q), sediment fluxes ( $Q_s$ ), and  $Q/Q_s$ 947 ratios between the Delft3D model and the Panther Tongue Delta because the trunk stream of the Panther 948 Tongue Delta is not exposed in outcrop, but the model results are scalable. By testing the model 949 predictions against the Goose River Delta, which itself has different water depths, discharges, sediment

950 fluxes, and  $Q/Q_s$  ratios, we validated that the model results are scalable to some extent, and can therefore 951 reasonably be applied to the Panther Tongue Delta.

952 For basin depths between 20 m and 30 m, Delft3D modelling predicts average clinoform dip magnitudes ranging from 0.74° and 1.1°, and foreset dip azimuth variability ranging from 0.37 to 0.31, 953 954 respectively. The observed clinoform dip magnitude  $(4.4^{\circ})$  is within a factor of four of the predicted 955 value while the observed foreset dip azimuth variability (0.53) is within a factor of two (Table 2). It is 956 worth noting that the basin depth of the Panther Tongue Mbr. is similar to that of the Goose River Delta 957 (~30 m) and both deltas possess average of clinoform dip magnitudes between 4° and 5°. This 958 consistency suggests that basin depth may be a reasonable predictor of clinoform dip magnitude in the 959 field, and that the Delft3D simulations tend to underestimate clinoform dip magnitudes. Increasing 960 clinoform dip magnitudes from proximal to distal are consistent within an increase in water depth from 961 proximal to distal. The discrepancy between the predicted and observed foreset dip azimuth variability 962 may be due to the Panther Tongue Delta prograding into slightly shallower water across the whole basin, 963 regardless of any difference between proximal and distal water depths. The disparity could also be due 964 to the small sample size (N=11) of the observed foreset dip azimuth data. Limited exposures are 965 inherently a problem in outcrop studies, and the observed data may not have provided a representative 966 value of the foreset dip azimuth variability for the Panther Tongue Mbr.

967 The similarity of the average clinoform dip magnitude in the Panther Tongue Mbr. and Goose
968 River Delta suggests that the estimates of basin depth are reasonable estimates for portions of the
969 Panther Tongue Delta. Earlier workers speculated that the higher magnitude clinoform dips in the
970 southern part of the Panther Tongue are part of a different lobe than the clinoforms located near Helper,
971 UT (Hwang and Heller, 2002; Hampson, Gani et al., 2011). We agree with the interpretation that this is
972 a separate delta lobe. The increased mean grain size and clinoform dips are inconsistent with the delta-

973 front facies observed in the proximal, northern portion of the Panther Tongue Mbr., and indicate a 974 change in the forcings experienced by the delta as one might expect in a separate lobe formed at a 975 different time. Hwang and Heller (2002) have suggested that an increased wave climate caused the 976 higher clinoform dips in the southern lobe. We propose an alternative hypothesis: the change in 977 clinoform dip could also be due to the Panther Tongue Delta prograding into progressively deeper water, 978 and that BLF is not a necessary condition for this change in clinoform dip magnitude to arise. Our 979 hypothesis is consistent with Delft3D modelling results indicating that basin depth is more highly 980 correlated with steeper clinoform dip magnitudes than BLF. If true, then the southern lobe of the 981 Panther Tongue Delta should possess fewer active distributaries, a longer avulsion period, smaller 982 average lobe areas, lower initial topset/foreset ratios (not considering the subsequent ravinement), and a 983 more rugose shoreline than would be present in the proximal portions of the Panther Tongue Mbr. where 984 water depths were shallower.

985 The Delft3D modelling presented here assumes there is no wave or tide influence on the 986 simulated deltas, so it is important to consider the effects of waves and tides might have had on the 987 Panther Tongue Delta. Waves would cause littoral drift along the delta front and inhibit river mouth bar 988 formation, causing fewer active distributaries. Littoral drift would smooth the shoreline as well and 989 decrease the shoreline rugosity. Wave winnowing could result in removal of fine grain sediments 990 leaving only coarser grains in the delta foreset. These coarser grains may then result in a steeper 991 clinoform dip magnitude. This lends credibility to the hypothesis of Hwang and Heller (2002) that the 992 southern lobe of the Panther Tongue is coarser with steeper clinoforms due to increased wave influence, 993 but it does not rule out our own hypothesis that the Panther Tongue Delta was prograding into deeper 994 water. Tide action would also inhibit mouth bar formation and therefore result in fewer active

distributaries. Tides could potentially create more rugose shorelines complex delta fronts. There is littleevidence for tide influence on the Panther Tongue, however.

997 In summary, Delft3D predictions of average clinoform dip magnitude and foreset dip azimuth 998 variability are a reasonable fit with observed values. The Goose River Delta and Panther Tongue Mbr. 999 probably prograded into similar water depths, and consequently, contain clinoforms of similar dip 1000 magnitudes. We interpret the southern region of the Panther Tongue Mbr. with steep clinoform dips to 1001 be a separate delta lobe. We propose that the steeper clinoform dips in the southern exposures are the 1002 result of the Panther Tongue Delta prograding into deeper water, and not necessarily experiencing BLF. 1003 We conjecture that the southern lobe of the Panther Tongue Delta possessed fewer active distributaries, 1004 a longer avulsion period, smaller average lobe areas, lower initial topset/foreset ratios, and a more 1005 rugose shoreline than the more proximal, northern lobe of the Panther Tongue Delta where the water 1006 depth was shallower.

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### 1008 **Conclusions**

1010 Delft3D simulations predict a range of morphometries for medium-sized, coarse-grained deltas 1011 prograding on shelves of very shallow to medium depths and under various rates of BLF. Deep basins 1012 experiencing high rates of BLF produce deltas with steep, negative shoreline trajectories, fewer active 1013 distributaries and longer avulsion periods. The result is a more rugose shoreline. Deeper initial basin 1014 depths are also associated with smaller average lobe areas, smaller topset/foreset ratios, less variability 1015 in foreset dip azimuths, and steeper clinoforms. We found that BLF alone is a good predictor of topset 1016 roughness and a delta's aspect ratio. Within our modelled parameter space, we saw no topset 1017 aggradation in any simulated delta with BLF. Additionally, we found that there is no change in mean 1018 grain size from proximal to distal. Model predictions of a delta's planform and internal geometry are

- 1019 consistent with the Goose River Delta in Labrador, Canada which is known to be experiencing 5 mm yr
- 1020 <sup>1</sup> of BLF. We applied our model to the Cretaceous Panther Tongue Mbr. in the Book Cliffs of Utah to
- 1021 re-evaluate the role of BLF in the formation of the Panther Tongue Delta. We have reinterpreted the
- 1022 Panther Tongue Delta's southern lobe be to prograding into deeper water resulting in a steeper clinoform
- 1023 dip magnitudes, and that BLF was not a necessary condition for to cause this change in clinoform dip.
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- 1025

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1180	Appendix A
1181	Delft3D Setup Files for Simulated Delta in 4 m Water Depth and 10 mm yr <sup>-1</sup> BLF
1182	

1183 **MDF-File** 1184 4m 10mm final.mdf Ident = #Delft3D-FLOW . 03. 02 3. 42. 00. 17790# 1185 1186 Commut = 1187 Runtxt = #JAC 5/16/2014# 1188 #5grains D50 170um# 1189 #4m flat depth# #10mm/yr with 14 day# 1190 1191 #intermittency factor# 1192 #erosion factor 0.33# 1193 #sloping channel# 1194 Filcco = #. \5\_16Grid. grd# 1195 Anglat = 0.0000000e+0001196 Grdang = 0.000000e+000Filgrd = #..\5\_16Grid.enc# MNKmax = 584 338 1 1197 1198 1199 Thi ck = 1.000000e+0021200 Commut = Fildep = #.  $\land$  4m. dep# 1201 1202 Commnt = 1203 Commut = no. dry points: 01204 Commut = no. thin dams: 01205 Commut = 1206 Itdate = #2014 - 01 - 02#1207 Tunit = #M#1208 Tstart = 0.000000e+0001209 Tstop = 1.5782400e+0061210 Dt = 0.11211 Tzone = 01212 Commut = 1213 Sub1 = # # 1214 Sub2 = # C #1215 Namc1 = #SedimentNC275 #Namc2 = #SedimentNC250 #1216 1217 Namc3 = #SedimentNC150 #1218 Namc4 = #SedimentCOHO. 21931 #1219 Namc5 = #SedimentCOHO.05651 # 1220 Commut = 1221 Wnsvwp = #N#1222 Wndint = #Y#1223 Commut = 1224 Zeta0 = 0.000000e+0001225 C01 = 0.0000000e+0001226 C02 = 0.0000000e+0001227 C03 = 0.0000000e+0001228 C04 = 0.0000000e+0001229 C05 = 0.0000000e+0001230 Commut = 1231 Commut = no. open boundaries: 41232 Filbnd = #4m 10mm final.bnd# 1233 FilbcT = #4m 10mm final.bct# 1234 FilbcC = #4m 10mm final.bcc# 1235 Rettis = 0.0000000e+000

1236 0.000000e+000 1237 0.000000e+000 1238 0.000000e+000 Rettib = 0.0000000e+0001239 1240 0.000000e+000 0.000000e+0001241 1242 0.000000e+000 1243 Commut = 1244 Ag = 9.810000e+0001245 Rhow = 1.000000e+0031246 Tempw = 1.500000e+0011247 Salw = 3.100000e+0011248  $Wstres = 6.300000e-004 \ 0.000000e+000 \ 7.2300000e-003 \ 1.000000e+002$ 7. 2300000e-003 1. 0000000e+002 1249 1250 Rhoa = 1.0000000e+0001251 Betac = 5.000000e-0011252 Equili = #N#1253 Ktemp = 0Fclou = 0.000000e+0001254 1255 Sarea = 0.0000000e+000Temint = #Y#1256 1257 Commnt = 1258 Roumet = #C#1259 Ccofu = 6.500000e+0011260 Ccofv = 6.500000e+001Xl o = 0.000000e+0001261 1262 Vi couv = 1.000000e-0031263 Di couv = 1.000000e-003Htur2d = #Y#1264 1265 Page 1 4m 10mm final.mdf 1266 1267 Htural = 1.6666660e+0001268 Hturnd = 21269 Hturst = 7.000000e-0011270 Hturlp = 3.333330e-0011271 Hturrt = 1.000000e+0001272 Hturdm = 0.000000e+0001273 Hturel = #Y#1274 Irov = 0Filsed = #4m 10mm final.sed# 1275 1276 Filmor = #4m 10mm final.mor# 1277 Commnt = 1278 Iter = 2Dryflp = #YES#1279 1280 Dpsopt = #MAX#Dpuopt = #MOR# 1281 Dryflc = 1.000000e-0011282 Dco = 0.0000000e+0001283 1284 Tl fsmo = 6.000000e+001ThetQH = 0.000000e+0001285 1286 Forfuv = #Y#1287 Forfww = #N#1288 Sigcor = #N#Trasol = #Cyclic-method# 1289

1290	Momsol = #Cyclic#
1291	Commut =
1292	Commut = no. discharges: 0
1293	Commut = no. observation points: 1
1294	Filsta = #4m_10mm_final.obs#
1295	Commut = no. drogues: 0
1296	Commut =
1297	Commut =
1298	Commut = no. cross sections: 1
1299	Filcrs = #4m_10mm_final.crs#
1300	Commt =
1301	SMhydr = #YYYYY#
1302	SMderv = #YYYYY#
1303	SMproc = #YYYYYYYY#
1304	PMhydr = #YYYYY#
1305	PMderv = #YYY#
1306	PMproc = #YYYYYYYY#
1307	SHhydr = #YYYY#
1308	SHderv = #YYYYY#
1309	SHproc = #YYYYYYYY#
1310	SHflux = #YYYY#
1311	PHhydr = #YYYYYY#
1312	PHderv = #YYY#
1313	PHproc = #YYYYYYYY#
1314	PHf1 ux = #YYYH
1315	Onl i ne = #N#
1316	$FI map = 0.000000e+000 \ 60 \ 1.5782400e+006$
1317	$Fl his = 0.000000e+000 \ 0 \ 1.5782400e+006$
1318	Fl pp = 0.000000e+000 0 0.000000e+000
1319	FIrst = 1440
1320	Commut =
1321	Commut =
1322	

## BND-file

- 4m\_10mm\_final.bnd

- east Z T 584 337 584 2 0.0000000e+000 north Z T 2 338 583 338 0.0000000e+000 west Z T 1 2 1 337 0.0000000e+000 feeder T T 291 1 295 1 0.0000000e+000 Uniform
- Page 1

1330 **BCC-file** 1331 4m 10mm final.mdf Ident = #Delft3D-FLOW . 03. 02 3. 42. 00. 17790# 1332 1333 Commut = 1334 Runtxt =  $\#JAC \ 5/16/2014\#$ 1335 #5grains D50 170um# 1336 #4m flat depth# 1337 #10mm/yr with 14 day# 1338 #intermittency factor# 1339 #erosion factor 0.33# 1340 #sloping channel# 1341 Filcco = #.  $\sum 16Grid. grd #$ 1342 Anglat = 0.0000000e+0001343 Grdang = 0.000000e+000Filgrd = #..\5\_16Grid.enc# MNKmax = 584 338 1 1344 1345 1346 Thi ck = 1.000000e+0021347 Commut = Fildep = #.  $\land$  4m. dep# 1348 1349 Commnt = 1350 Commut = no. dry points: 01351 Commut = no. thin dams: 01352 Commut = Itdate = #2014 - 01 - 02#1353 1354 Tunit = #M#1355 Tstart = 0.000000e+0001356 Tstop = 1.5782400e+0061357 Dt = 0.11358 Tzone = 01359 Commut = 1360 Sub1 = # # Sub2 = # C #1361 1362 Namc1 = #SedimentNC275 #Namc2 = #SedimentNC250 #1363 1364 Namc3 = #SedimentNC150 #1365 Namc4 = #SedimentCOH0. 21931 # Namc5 = #SedimentCOHO.05651 # 1366 1367 Commut = Wnsvwp = #N#1368 1369 Wndint = #Y#1370 Commut = 1371 Zeta0 = 0.000000e+000C01 = 0.0000000e+0001372 1373 C02 = 0.0000000e+0001374 C03 = 0.0000000e+0001375 C04 = 0.0000000e+0001376 C05 = 0.0000000e+0001377 Commut = 1378 Commut = no. open boundaries: 4Filbnd = #4m\_10mm\_final.bnd# 1379 FilbcT = #4m 10mm final.bct# 1380 FilbcC = #4m 10mm final.bcc# 1381 1382 Rettis = 0.0000000e+000

1383 0.000000e+000 1384 0.000000e+000 1385 0.000000e+000 Rettib = 0.0000000e+0001386 1387 0.000000e+000 0.000000e+0001388 1389 0.000000e+000 1390 Commut = 1391 Ag = 9.810000e+0001392 Rhow = 1.000000e+0031393 Tempw = 1.500000e+0011394 Salw = 3.100000e+0011395  $Wstres = 6.300000e-004 \ 0.000000e+000 \ 7.2300000e-003 \ 1.000000e+002$ 1396 7. 2300000e-003 1. 0000000e+002 1397 Rhoa = 1.0000000e+0001398 Betac = 5.000000e-0011399 Equili = #N#1400 Ktemp = 0Fclou = 0.000000e+0001401 1402 Sarea = 0.0000000e+0001403 Temint = #Y#1404 Commut = 1405 Roumet = #C#Ccofu = 6.500000e+0011406 1407 Ccofv = 6.500000e+001Xl o = 0.000000e+0001408 1409 Vi couv = 1.000000e-0031410 Di couv = 1.000000e-0031411 Htur2d = #Y#1412 Page 1 4m 10mm final.mdf 1413 1414 Htural = 1.6666660e+0001415 Hturnd = 2Hturst = 7.000000e-0011416 Hturlp = 3.333330e-0011417 1418 Hturrt = 1.000000e+0001419 Hturdm = 0.000000e+0001420 Hturel = #Y#Irov = 01421 1422 Filsed = #4m 10mm final.sed# 1423 Filmor = #4m 10mm final.mor# 1424 Commut = 1425 Iter = 21426 Dryflp = #YES#1427 Dpsopt = #MAX#Dpuopt = #MOR#1428 Dryflc = 1.000000e-0011429 1430 Dco = 0.0000000e+0001431 Tl fsmo = 6.000000e+001ThetQH = 0.000000e+0001432 1433 Forfuv = #Y#1434 Forfww = #N#1435 Sigcor = #N#Trasol = #Cyclic-method# 1436

1437	Momsol = #Cyclic#
1438	Commut =
1439	Commut = no. discharges: 0
1440	Commut = no. observation points: 1
1441	Filsta = #4m_10mm_final.obs#
1442	Commut = no. drogues: 0
1443	Commut =
1444	Commut =
1445	Commut = no. cross sections: 1
1446	Filcrs = #4m_10mm_final.crs#
1447	Commut =
1448	SMhydr = #YYYYY#
1449	Smderv = #YYYYY#
1450	Smproc = #YYYYYYYY#
1451	Pmhydr = #YYYYYY#
1452	Pmderv = #YYY#
1453	Pmproc = #YYYYYYYY#
1454	Shhydr = #YYYY#
1455	Shderv = #YYYYY#
1456	Shproc = #YYYYYYYY#
1457	Shflux = #YYYY#
1458	Phhydr = #YYYYY#
1459	Phderv = #YYY#
1460	Phproc = #YYYYYYYY#
1461	Phflux = #YYYY#
1462	Onl ine = #N#
1463	$FI map = 0.000000e+000 \ 60 \ 1.5782400e+006$
1464	$Fl his = 0.000000e+000 \ 0 \ 1.5782400e+006$
1465	$FIpp = 0.000000e+000 \ 0.000000e+000$
1466	Flrst = 1440
1467	Commut =
1468	Commut =
1469	

1470 **BCT-file** 1471 4m 10mm final.bct 1472 table-name 'Boundary Section : 1' contents 'Uniform' location 'east ' 1473 1474 1475 time-function 'non-equidistant' 1476 reference-time 20140102 time-unit 'minutes' 1477 1478 interpolation 'linear' 1479 parameter 'time ' unit '[min]' parameter 'water elevation (z) end A' unit '[m]' 1480 parameter 'water elevation (z) end B' unit '[m]' 1481 1482 records-in-table 2 1483 0.000000e+000 0.000000e+000 0.000000e+000 1484 1. 5782400e+006 - 3. 9107140e+002 - 3. 9107140e+002 table-name 'Boundary Section : 2' 1485 contents 'Uniform 1486 location 'north 1487 1488 time-function 'non-equidistant' 1489 reference-time 20140102 1490 time-unit 'minutes' 1491 interpolation 'linear' parameter 'time ' unit '[min]' 1492 1493 parameter 'water elevation (z) end A' unit '[m]' 1494 parameter 'water elevation (z) end B' unit '[m]' 1495 records-in-table 2 1496 0.000000e+000 0.000000e+000 0.000000e+000 1497 1. 5782400e+006 - 3. 9107140e+002 - 3. 9107140e+002 table-name 'Boundary Section : 3' 1498 contents 'Uniform location 'west ' 1499 1500 1501 time-function 'non-equidistant' reference-time 20140102 1502 1503 time-unit 'minutes' 1504 interpolation 'linear' 1505 parameter 'time ' unit '[min]' parameter 'water elevation (z) end A' unit '[m]' 1506 parameter 'water elevation (z) end B' unit '[m] 1507 1508 records-in-table 2 1509 0.000000e+000 0.000000e+000 0.000000e+000 1510 1. 5782400e+006 - 3. 9107140e+002 - 3. 9107140e+002 1511 table-name 'Boundary Section : 4' contents 'Uniform 1512 location 'feeder 1513 1514 time-function 'non-equidistant' 1515 reference-time 20140102 1516 time-unit 'minutes' 1517 interpolation 'linear' 1518 parameter 'time ' unit '[min]' parameter 'total discharge (t) end A' unit '[m3/s]' 1519 parameter 'total discharge (t) end B' unit '[m3/s]' 1520 1521 records-in-table 2 1522 0.000000e+000 1.000000e+003 9.9999900e+002

**1.5782400e+006 1.000000e+003 9.9999900e+002**  1525 MOR-file 1526 4m 10mm final.mor [MorphologyFileInformation] 1527 FileCreatedBy = Delft3D FLOW-GUI, Version: 3.42.00.17790 1528 1529 FileCreationDate = Fri May 16 2014, 17:09:581530 FileVersion = 02.001531 [Morphology] 1532 EpsPar = false Vertical mixing distribution according to van Rijn 1533 (overrules k-epsilon model) 1534 IopKCW = 1 Flag for determining Rc and Rw 1535 RDC = 0.01 [m] Current related roughness height (only used if IopKCW 1536 <> 1) RDW = 0.02 [m] Wave related roughness height (only used if IopKCW <> 1537 1538 1) 1539 MorFac = 5.0000000e+002 [-] Morphological scale factor MorStt = 3.6000000e+002 [min] Spin-up interval from TStart till start 1540 1541 of 1542 morphological changes 1543 Thresh = 5.0000001e-002 [m] Threshold sediment thickness for 1544 transport and 1545 erosion reduction 1546 MorUpd = true Update bathymetry during FLOW simulation 1547 EqmBc = false Equilibrium sand concentration profile at inflow 1548 boundari es 1549 DensIn = false Include effect of sediment concentration on fluid 1550 density 1551 AksFac = 1.0000000e+000 [-] van Rijn's reference height = AKSFAC \* KS RWave = 2.0000000e+000 [-] Wave related roughness = RWAVE \* estimated 1552 1553 ripple height. Van Rijn Recommends range 1-3 1554 1555 AlfaBs = 1.0000000e+000 [-] Streamwise bed gradient factor for bed 1556 load transport 1557 AlfaBn = 1.5000000e+000 [-] Transverse bed gradient factor for bed 1558 load transport 1559 Sus = 1.0000000e+000 [-] Multiplication factor for suspended sediment reference concentration 1560 1561 Bed = 1.0000000e+000 [-] Multiplication factor for bed-load transport 1562 vector 1563 magni tude 1564 SusW = 1.0000000e+000 [-] Wave-related suspended sed. transport 1565 factor 1566 BedW = 1.0000000e+000 [-] Wave-related bed-load sed. transport factor SedThr = 1.0000000e-001 [m] Minimum water depth for sediment 1567 1568 computations 1569 ThetSD = 3.3000000e-001 [-] Factor for erosion of adjacent dry cells HMaxTH = 1.5000000e+000 [m] Max depth for variable THETSD. Set < 1570 SEDTHR to use 1571 1572 global value only FWFac = 1.0000000e+000 [-] Vertical mixing distribution according to 1573 1574 van Riin 1575 (overrules k-epsilon model) 1576 [Output] 1577 SourceSinkTerms = True

Bedslope = True Frac = True MudFrac = True Percentiles = True HidExp = True Bedforms = True Dm = True Dg = True[UnderLayer] I UnderLyr = 2 MxNuLyr = 100 TTLForm = 1 ThTrLyr = 0.2ThUnl yr = 0.1UpdBaseLyr = 1

```
1594
                                         SED-file
1595
      4m 10mm final.sed
1596
       [SedimentFileInformation]
1597
      FileCreatedBy = Delft3D FLOW-GUI, Version: 3.42.00.17790
1598
      FileCreationDate = Fri May 16 2014, 17:09:57
1599
      FileVersion = 02.00
1600
      [SedimentOverall]
      Cref = 1.6000000e+003 [kg/m3] CSoil Reference density for hindered
1601
1602
      settling
1603
      cal cul ati ons
      IopSus = 0 If Iopsus = 1: susp. sediment size depends on local
1604
1605
      flow and wave conditions
1606
      [Sediment]
1607
      Name = #SedimentNC275# Name of sediment fraction
      SedTyp = sand Must be "sand", "mud" or "bedload"
1608
      RhoŠol = 2.6500000e+003 [kg/m3] Specific density
1609
      SedDia = 2.7500000e-004 [m] Median sediment diameter (D50)
1610
      CDryB = 1.600000e+003 [kg/m3] Dry bed density
1611
      IniŠedThick = 1.0000000e+001 [m] Initial sediment layer thickness at
1612
1613
      bed (uniform
1614
      value or filename)
1615
      FacDSS = 1.0000000e+000 [-] FacDss * SedDia = Initial suspended
      sediment
1616
1617
      diameter. Range [0.6 - 1.0]
1618
       [Sediment]
      Name = #SedimentNC250# Name of sediment fraction
SedTyp = sand Must be "sand", "mud" or "bedload"
1619
1620
1621
      RhoSol = 2.6500000e+003 [kg/m3] Specific density
1622
      SedDia = 2.5000000e-004 [m] Median sediment diameter (D50)
      CDryB = 1.6000000e+003 [kg/m3] Dry bed density
1623
1624
      IniSedThick = 2.5000000e+001 [m] Initial sediment layer thickness at
1625
      bed (uniform
1626
      value or filename)
      FacDSS = 1.0000000e+000 [-] FacDss * SedDia = Initial suspended
1627
1628
      sediment
1629
      diameter. Range [0.6 - 1.0]
1630
       [Sediment]
1631
      Name = #SedimentNC150# Name of sediment fraction
      SedTyp = sand Must be "sand", "mud" or "bedload"
1632
      RhoSol = 2.6500000e+003 [kg/m3] Specific density
SedDia = 1.5000000e-004 [m] Median sediment diameter (D50)
1633
1634
      CDryB = 1.6000000e+003 [kg/m3] Dry bed density
1635
      IniSedThick = 3.000000e+001 [m] Initial sediment layer thickness at
1636
1637
      bed (uniform
1638
      value or filename)
      FacDSS = 1.0000000e+000 [-] FacDss * SedDia = Initial suspended
1639
1640
      sediment
1641
      diameter. Range [0.6 - 1.0]
1642
       [Sediment]
      Name = #SedimentCOHO. 21931# Name of sediment fraction
1643
      SedTyp = mud Must be "sand", "mud" or "bedload"
1644
      RhoŠol = 2.6500000e+003 [kg/m3] Specific density
1645
1646
      SalMax = 0.0000000e+000 [ppt] Salinity for saline settling velocity
```

1647 WS0 = 2.1931000e-004 [m/s] Settling velocity fresh water WSM = 2.1931000e-004 [m/s] Settling velocity saline water 1648 1649 TcrSed = 1.0000000e+003 [N/m2] Critical bed shear stress for sedimentation (uniform 1650 1651 value or filename) TcrEro = 5.0000000e-001 [N/m2] Critical bed shear stress for erosion 1652 1653 (uni form 1654 value or filename) 1655 EroPar = 1.000000e-004 [kg/m2/s] Erosion parameter (uniform 1656 value or filename) CDrvB = 5.000000e+002 [kg/m3] Dry bed density 1657 1658 IniŠedThick = 1.0000000e+001 [m] Initial sediment layer thickness at 1659 bed (uniform 1660 value or filename) FacDSS = 1.0000000e+000 [-] FacDss \* SedDia = Initial suspended 1661 1662 sediment diameter. Range [0.6 - 1.0] 1663 1664 [Sediment] Name = #SedimentCOHO. 05651# Name of sediment fraction 1665 SedTyp = mud Must be "sand", "mud" or "bedload" 1666 RhoSol = 2.6500000e+003 [kg/m3] Specific density 1667 SalMax = 0.0000000e+000 [ppt] Salinity for saline settling velocity 1668 WSO = 5.6510000e-005 [m/s] Settling velocity fresh water WSM = 5.6510000e-005 [m/s] Settling velocity saline water 1669 1670 TcrSed = 1.0000000e+003 [N/m2] Critical bed shear stress for 1671 1672 sedimentation (uniform 1673 value or filename) 1674 TcrEro = 5.0000000e-001 [N/m2] Critical bed shear stress for erosion 1675 (uni form 1676 value or filename) 1677 EroPar = 1.000000e-004 [kg/m2/s] Erosion parameter (uniform 1678 value or filename) CDrvB = 5.000000e+002 [kg/m3] Dry bed density 1679 1680 IniŠedThick = 1.0000000e+001 [m] Initial sediment layer thickness at bed (uniform 1681 1682 value or filename) FacDSS = 1.0000000e+000 [-] FacDss \* SedDia = Initial suspended 1683 1684 sedi ment 1685 1686 diameter. Range [0.6 - 1.0]

1687 FIL-file 1688 4m 10mm final.fil Domain, Checked : No 1689 Grid :  $.. \ 5_{16}$ Grid. grd 1690 Grid enclosure : ... \5\_16Grid. enc 1691 1692 Bathymetry : ... \4m. dep Dry points : none 1693 Thin dams : none 1694 1695 Time frame, Checked : No 1696 Processes, Checked : No 1697 Initial conditions, Checked : No Boundaries, Checked : Yes 1698 1699 Boundary definitions : 4m 10mm final.bnd Astronomical flow conditions : none 1700 Astronomical corrections : none 1701 1702 Harmonic flow conditions : none 1703 OH-relation flow conditions : none 1704 Time series flow conditions : 4m 10mm final.bct 1705 Transport conditions : 4m\_10mm\_final.bcc Physical parameters, Checked : No 1706 1707 Roughness coefficients : none Hor. viscosity/diffusivity : none 1708 Heat flux model data : none 1709 1710 Sediment data : 4m 10mm final.sed 1711 Morphology data : 4m\_10mm\_final.mor 1712 Uniform wind data : none Space varying wind data : none 1713 1714 Numerical parameters, Checked : No Operations, Checked : No 1715 Discharge definitions : none 1716 1717 Discharge data : none Dredging and dumping data : none 1718 Monitoring, Checked : No Observation points : 4m\_10mm\_final.obs 1719 1720 1721 Drogues : none 1722 Cross-sections : 4m\_10mm\_final.crs 1723 Additional parameters, Checked : No 1724 Output, Checked : No 1725 Fourier analysis data : none

1727	Appendix B
1728	
1729	MATLAB Scripts for Analyzing Delft3d Simulations
1730	

```
1731
                             Clinoform Dip Magnitude and Dip Direction Code
1732
       % Clinoform Dip Magnitudes for Delft3D Deltas
1733
       %
1734
       % Code modified from "clinodipsver07062011" created by RLS and APB
1735
       % APB April 17, 2012
1736
         Modified by ABM to account for base level change November 10, 2012
       %
1737
       % Modified by JAC 2014
1738
       % NOTE: BE SURE TO CHANGE ALL VALUES IN CODE WHICH ARE RUN AND/OR TIME
1739
       % SPECIFIC BEFORE RUNNING!
1740
       88
1741
       clear all; close all; clc
1742
       %% USER ACTION REQUIRED
1743
       cd Y:\Cederberg\FinalDeltas data\4m5mm
1744
       % 1. Load bed elevation data stored in bedlevel.mat written from Quickplot:
1745
       load bedlevel.mat
1746
       % 2. Define timestep of interest for clinoform measurment:
1747
       TStep = 112;
1748
       %dts = 0; %Amount of base level change, in meters, in a single timestep(factoring
1749
       in the MSF)Positive values relate to RBL Fall, negative to RBL Rise
1750
       dts=0.007440475646880;%5mm
1751
       %dts=0.014880951293760;%10mm%% NO ACTION REQUIRED
1752
       % 3. Extract the bed elevation for a timestep (the timetep is the first
1753
       % number in the array counters)
1754
       Z=data.Val(TStep,:,:);
1755
       ZZ=squeeze(Z);
1756
       [row,col]=size(ZZ);
1757
       % We rotate the delta to prograde to the north because it makes the
1758
       % extraction of the clinoform slopes easier. But note that this reverses
1759
       % the counters in the matrix. The "flipdim" line corrects the error that
1760
       % results from bringing the Delft image from Delft to MatLab. The image
1761
       % will come into MatLab as the mirror image of the Delft image.
1762
       ZZ=flipdim(ZZ,1);
1763
       ZZ=rot90(ZZ,3);
1764
       dem=ZZ;
1765
       dim = size(ZZ);
1766
       N=dim(2);
1767
       contour(ZZ,30)
1768
       caxis([-20 3])
1769
       hold on
1770
       % 4. Contour the shoreline (actually the -0.1 m contour)as thick black line
1771
       v=[-0.1-(dts*(TStep-1))];
1772
       contour(ZZ,v,'k','LineWidth', 2)
1773
       caxis([-20 3])
1774
       % 5. Now define the region of the delta from which you want bed (clinoform
1775
       % surface) slopes. Generally we want to exclude the top- and bottom-set
1776
       % region. Extract the bed elevations and bed slopes of interest by setting
1777
       % all bed elevations and slopes landward of the region of interest to 0:
1778
       for j = 1:320
1779
           for i = 1:220
1780
           if ZZ(i,j) \ge -0.10 %Eliminates the topset, except for channels
1781
               ZZ(i,j) = NaN;
1782
           elseif i < 30
1783
               ZZ(i,j) = NaN;
                               %Eliminates the feeder channel and non-deltaic
1784
                                %shoreline; This line number (30) may change with
1785
                                %different deltas
1786
           end
```

```
1787
           end
1788
       end
1789
       %% USER ACTION REQUIRED
1790
       % 6. Define the toes of the delta clinoform. Hit enter when done. Be sure
1791
       % your line extends from x=0 to x=xmax and all x values are unique.
1792
       [X,Y]=ginput;
1793
       X=round(X);
1794
       Y=round(Y);
1795
       XX=1:N;
1796
       YY = interpl(X,Y,XX,'linear');
1797
       hold on
1798
       YY=round(YY);
1799
       plot(XX,YY,'*')
1800
       % 7. Define the topset region from which you want to remove bed elevations
1801
       % associated with channels. Be sure your line extends from x=0 to x=xmax
1802
       % and all x values are unique.
1803
       [Xtop,Ytop]=ginput;
1804
       Xtop=round(Xtop);
1805
       Ytop=round(Ytop);
1806
       XXtop=1:N;
1807
       YYtop = interp1(Xtop,Ytop,XXtop,'linear');
1808
       hold on
1809
       YYtop=round(YYtop);
1810
       plot(XXtop,YYtop,'o')
1811
       drawnow
1812
       % Make a vector of zeros and ones, with ones where YYtop is a NaN to
1813
       % control the loops below
1814
       ControlVec = isnan(YYtop);
1815
       % Extract the bed elevations and bed slopes of interest by setting all
1816
       % elevations and slopes seward of the region of interest to 0
1817
       for j = 1:row
1818
           for i = 1:col
1819
           if i > YY(j)
1820
               ZZ(i,j) = NaN;
1821
           end
1822
           if ControlVec(j) ~= 1 && i < YYtop(j)</pre>
1823
               ZZ(i,j) = NaN;
1824
           end
1825
           end
1826
       end
1827
       % Contour the bathymetry of the delta clinoform in the region of study
1828
       hold off
1829
       subplot(2,2,1); contour(dem,30);
1830
       subplot(2,2,2); [CS, H] = contour(ZZ,30);
1831
       %%
1832
       % 8. Calculate the aspect (dip direction), slope, and gradients (along the
1833
       % axes) of the delta foreset at every Delft3D cell. The reference vector
1834
       % converts the bathy elevation matric to actual geographic coordinates.
1835
       % The first number in the vector is the only important one; it gives the
1836
       % number of matrix entries per degree latitude. Because our spacing is 25
1837
       % m, and there are 111000 meters per degree, the number of cells for us is
1838
       % 111000/25.
1839
       refvec = [111000/25 0 0];
1840
       [ASPECT, SLOPE, gradN, gradE] = gradientm(ZZ, refvec);
1841
       % Convert the aspect from a matrix to a column vector, while converting
1842
       % aspect to radians
1843
       k=0;
```

```
1844
       for i=1:col
1845
           for j=1:row
1846
               k=k+1;
1847
               theta(k) = pi/180*ASPECT(i,j);
1848
               dip(k) = SLOPE(i,j);
1849
           end
1850
       end
1851
       % Remove NaNs
1852
       theta(isnan(theta)) = [];
1853
       dip(isnan(dip)) = [];
1854
       %Remove all slope data from the area of interest that are of a value less
1855
       %than what is observed in a foreset.
1856
       dimdip=size(dip);
1857
       increm = 0;
1858
       for counter=1:dimdip(2);
1859
           if dip(counter) >= 0.008; % Modified from 0.08 to 1 by JAC 3/26/2014
1860
               increm = increm+1;
1861
               newdip(increm) = dip(counter);
1862
               newtheta(increm)=theta(counter);
1863
           end
1864
       end
1865
       newtheta=sort(newtheta);
1866
       % 9. Plot a rose diagram of clinoform dip direction:
1867
       subplot(2,2,3);
1868
       nbins = 36;
1869
       h=rose(newtheta, nbins);
1870
       view(90,-90)
1871
       % Define some constants
1872
       num=size(newtheta);
1873
       x=0;
1874
       v=0;
1875
       % Calculate the mean dip direction and dispersion (the statistics below are
1876
       % derived from Doornkamp and King, 1971, "Numerical Analysis in
1877
       % Geomorphology", p. 208-213)
1878
       % VERSION 2 (from Jones, 2006)
1879
       C = sum(cos(newtheta));
1880
       S = sum(sin(newtheta));
1881
       cd Y:\Cederberg\Stats\MatLabStatPrograms\Vector Stats;
1882
       thetabar = VectMean_arctan(S,C); % function from Jones
1883
       R = sqrt((S/(num(2))^2 + (C/num(2))^2))
1884
       % Large Rbar = small variance and vice versa
1885
       s1 = sqrt(2*(1-R)); % Angular dispersion (in radians)as given by Doornkamp
1886
                            % and King
1887
       AngularDispersionDeg=s1*(180/pi)%Angular Dispersion in degrees
1888
       % Be sure that dip magnitude is in degrees:
1889
       dipdegrees = newdip;
1890
       newtheta=newtheta';
1891
       title(['Mean dip direction =',num2str(thetabar)],'FontSize',8)
1892
       subplot(2,2,4);
1893
       histbin=[0:0.05:20];
1894
       hist(newdip,histbin);
1895
       avedipmag=mean(dipdegrees)
1896
       stdev = std(dipdegrees)
1897
       p50=prctile(dipdegrees, 50)
1898
1899
       samples=length(dipdegrees);
1900
       text(50,500,['median dip magnitude =',num2str(p50)],'FontSize',8);
```

```
1901 text(10,20,['mean dip magnitude =',num2str(avedipmag)],'FontSize',8);
1902 text(10,100,['dip std dev =',num2str(stdev)],'FontSize',8);
1903 %text(10,80,['p95 dip =',num2str(p95)],'FontSize',8);
1904 %text(10,110,['Number of Samples =',num2str(samples)],'FontSize',8);
1905 title('Mean Clinoform Bed Dip')
1906 xlabel('dip (dg)')
1907 ylabel('Frequency by Number')
1908
```

```
1909
                                           Topset Roughness
1910
       %% Topset Roughness Code
1911
       % This code calculates the standard deviation of all elevation in the
1912
       % topset above 0.1m
1913
       %JAC 2014
1914
1915
       clear all; close all
1916
       cd ('Y:\Cederberg\finalDeltas_data\20m10mm\')% RUN-SPECIFIC
1917
       %dts = 0; %Amount of base level change, in meters, in a single
1918
       %timestep(factoring in the MSF)Positive values relate to RBL Fall,
1919
       %negative to RBL Rise
1920
       %dts=0.007440475646880;%5m
1921
       dts=0.014880951293760;%10mm
1922
       load bedlevel.mat
1923
       [t,r,c]=size(data.Val);
1924
       tmax=532;
1925
       ZZ=cell(1,tmax);
1926
       stdev=zeros(1,tmax);
1927
       for n=1:tmax
1928
           Z=[];
1929
           disp(['Computing time slice ' num2str(n)])
1930
           shore=-0.1-((i-1)*dts); %find the shoreline
1931
           for i=1:r
1932
               for j=1:c
1933
                    if data.Val(n,i,j)>(shore) & data.Val(n,i,j)<3 %Select points
1934
                                                               %within the shoreline
1935
                        Z=[Z data.Val(n,i,j)];
1936
                    end
1937
1938
               end
1939
           end
1940
           ZZ\{n\}=Z;
1941
           stdev(n)=std(ZZ{n}); %Calculate Std Dev
1942
       end
1943
       plot(stdev)
1944
       save('stdev','stdev')
1945
```
1946 Mean Grain Size and Topset Area of Each Delta Lobe 1947 %% Average Grain Size of Lobes and Average Lobe Size 1948 %Delineated lobes interactively with Matlab/Quickplot interface and 1949 %calculate meand grain size and area of each delta lobe 1950 %JAC 2014 1951 close all 1952 clear all 1953 clc 1954 %% This code is used for defining delta lobes in quickplot/matlab and calculating 1955 % the average and D50 grain size of the lobe 1956 1957 %open quickplot through matlab using d3d\_qp command 1958 %navigate to run 1959 d3d qp 1960 %% RUN SPECIFIC 1961 tstep=217; %SET TIME STEP of interest 1962 lyr=100;%number of strat layers 1963 d3d\_qp('openfile','H:\25mFinalRuns\8m10mmfinal\trim-8m\_10mm\_final.dat') 1964 d3d\_qp('selectfield','bed level in water level points') 1965 d3d\_qp('editt',tstep) 1966 d3d\_qp('loaddata') 1967 d3d qp('quickview') 1968 %% User Action Required, click around the lobe 1969 % Copy and paste as many times as needed to define all lobes 1970 % Make sure to rename marked lines 1971 a=impoly;%%Rename 'a' if needed 1972 pos=getPosition(a);%%Rename 'a' if needed 1973 xv = pos(:, 1);1974 yv = pos(:, 2);1975 X(:,:) = data.X(3:584,2:337);1976 Y(:,:) = data.Y(3:584,2:337);1977 IN=inpolygon(X,Y,xv,yv); 1978 areapixA=nnz(IN); 1979 volumepixA=areapixA\*lyr;%multiply the area by the number to strat layers 1980 %%RUN SPECIFIC 1981 cd G:\CEDERBERG\Delft\_Runs\12m0mmfinal 1982 load strat\_mm 1983 for i=2:101 1984 lobestrat(:,:,i)=IN.\*strat(:,:,i); 1985 end 1986 SumStratX=sum(lobestrat); 1987 SumStratX=squeeze(SumStratX); 1988 SumStratY=sum(SumStratX); 1989 SumStratY=squeeze(SumStratY); 1990 SumStrat=sum(SumStratY); 1991 AvgD50A=SumStrat/volumepixA;%%Rename 'AvgD50A' if needed 1992 %% Lobe2 1993 b=impoly;%%Rename 'a' if needed 1994 pos=getPosition(b);%%Rename 'a' if needed 1995 xv=pos(:,1); 1996 yv=pos(:,2); 1997 X(:,:) = data.X(3:584,2:337);1998 Y(:,:) = data.Y(3:584,2:337);1999 IN=inpolygon(X,Y,xv,yv); 2000 areapixB=nnz(IN); 2001 volumepixB=areapixB\*lyr; % multiply the area by the number to strat layers

```
2002
       %%RUN SPECIFIC
2003
       %cd H:\25mFinalRuns\8m10mmfinal\
2004
       %load strat_mm.mat
2005
       for i=2:101
2006
       lobestrat(:,:,i)=IN.*strat(:,:,i);
2007
       end
2008
       SumStratX=sum(lobestrat);
2009
       SumStratX=squeeze(SumStratX);
2010
       SumStratY=sum(SumStratX);
2011
       SumStratY=squeeze(SumStratY);
2012
       SumStrat=sum(SumStratY);
2013
       AvgD50B=SumStrat/volumepixB;%%Rename 'AvgD50A' if needed
2014
       %% Lobe 3
2015
       c=impoly;%%Rename 'a' if needed
2016
       pos=getPosition(c);%%Rename 'a' if needed
2017
       xv=pos(:,1);
2018
       yv=pos(:,2);
2019
       X(:,:) = data.X(3:584,2:337);
2020
       Y(:,:) = data.Y(3:584,2:337);
2021
       IN=inpolygon(X,Y,xv,yv);
2022
       areapixC=nnz(IN);
2023
       volumepixC=areapixC*lyr;%multiply the area by the number to strat layers
2024
       %%RUN SPECIFIC
2025
       %cd H:\25mFinalRuns\8m10mmfinal\
2026
       %load strat_mm.mat
2027
       for i=2:101
2028
       lobestrat(:,:,i)=IN.*strat(:,:,i);
2029
       end
2030
       SumStratX=sum(lobestrat);
2031
       SumStratX=squeeze(SumStratX);
2032
       SumStratY=sum(SumStratX);
2033
       SumStratY=squeeze(SumStratY);
2034
       SumStrat=sum(SumStratY);
2035
       AvgD50C=SumStrat/volumepixC;%%Rename 'AvgD50A' if needed
2036
```

```
2037
                                          Shoreline Rugosity
2038
       %% Shoreline Extraction and Isoperimetric Quotient Calculation
2039
       %Added McGuffin's Base Level Fall adjustment
2040
       %APB June 14, 2012
2041
       %Modified by JAC 2014
2042
       % Modified from the following:
2043
       %% Previous codes
2044
       %this m-file takes a cube of topography data from Delft3D output and
2045
       %converts each delta into a shoreline using the Open Angle Method (Shaw, et
2046
       %al, 2008).
2047
2048
       %Code edited by APB and RLS 11/9/11
2049
       %Note: When the delta has prograded to the edge of one of the open
2050
       %boundaries, this code will not compute the shoreline on the landward side
2051
       %of where the delta has prograded beyond the open boundary.
2052
       22
2053
       % clear all;
2054
       % close all;
2055
       % clc
2056
       cd 'Y:\Cederberg\FinalDeltas_data\20m10mm' % for different runs, change the
2057
       % run number in this line, and in line 74 of code.
2058
       %%
2059
       tmax=532;
2060
       % 1. Enter the number of time seps recorded for run and amount of base level fall
2061
       in a time step(make sure to account for MSF)[RUN SPECIFIC]:
2062
       timeslices =532;% 1:tmax; %Range of timesteps recorded
2063
       %dts = 0; %Amount of base level change, in meters, in a single timestep(factoring
2064
       in the MSF)Positive values relate to RBL Fall, negative to RBL Rise
2065
       %dts=0.007440475646880;%5mm
2066
       dts=0.014880951293760;%10mm
2067
       22
2068
       % 2. Load bedlevel.mat "bed level in water level points" exported from
2069
         QUICKPLOT for all time steps:
       %
2070
       load bedlevel; %
2071
       filename = 'temp';
2072
       areapix=cell(1,tmax);
2073
       Results.Area=ones(1,tmax);
2074
       Results.Perimeter=ones(1,tmax);
2075
       Results.IQ=ones(1,tmax);
2076
       FluvSurface=cell(1,tmax);
2077
       22
2078
       %
          3. Enter the initial time step where morphodynamic change begins to
2079
       %
         occur, or the time step where you would like to begin
2080
         calculating the shoreline [RUN SPECIFIC]:
       8
2081
       for i=timeslices;
2082
           z=data.Val;
2083
           m = length(z(:,1,1));
2084
               disp(['Computing shoreline for ' filename ' time slice ' num2str(i)])
2085
               ztemp=squeeze(z(i,:,:));
2086
               [r,c]=size(ztemp);
2087
               ztemp=ztemp(2:r-1,2:c-1); %the '-1' and '2' is to get rid of the collar of
2088
       NaNs
2089
               [r,c]=size(ztemp);
2090
               mid=ceil(r/2);
2091
               ztemp(mid-10:mid+10,1)=1;
2092
               [r,c]=size(ztemp);
```

```
2093
               [row,col]=size(ztemp);
2094
               zz=ztemp<(-0.1-((i-1)*dts)); % the land/water interface is defined as the</pre>
2095
       -0.1 m contour
2096
               if nansum(nansum(zz))<50</pre>
2097
               shore{1,i} = 0;
2098
               else
2099
               n = 90;
2100
               cd 'H:\25mFinalRuns\ShorelineCode'
2101
               sl=Seaangles2(zz,n); %this calls the OAM script written by John Shaw, et al
2102
       2008 GRL
2103
               sl2=sparse(sl(2,:),sl(1,:),sl(3,:),r,c);
2104
               sl2=sl2+0;
2105
               angle = 25;
2106
               c=contourc(sl2,[angle,angle]); %this is the NN degree OAM contour,
2107
               % but the OAM method is imperfect and picks up other smaller,
2108
               % artifical shorelines. Thus, to find the real one we call contourc,
2109
               % which exports the (x,y) for a given contour level then we sort
2110
               % through that array and find the longest contour which is the shoreline
2111
               seplines(c);
2112
               % sep=sep(:,2:length(sep(1,:))); %this cuts off the first contour line
2113
               % which is the border of the image and not the shoreline
2114
               temp=sep(:,find(sep(1,:)==max(sep(1,:)))); %this returns the 3-row vector
2115
       of the
2116
               % longest contour line, which corresponds to the shoreline
2117
               c=c(:,temp(2):temp(3));
2118
               shoretemp=[c(1,:); c(2,:)];
2119
               shore=shoretemp; %this is the x coord of the shoreline at time i
2120
               % Plot the shoreline:
2121
               x = shore(1, :);
2122
               y=shore(2,:);
2123
               % To see both the delta and the shoreline, add the delta to the
2124
               % figure:
2125
               plot(x,y,'o')
2126
               hold on
2127
               contour(ztemp)
2128
               end
2129
              Save the shoreline file:
       %
          4.
2130
       cd 'Y:\Cederberg\FinalDeltas data\20m5mm\Shoreline'
2131
       name=([filename(1:length(filename)-4) '_' num2str(i) '_OAM' num2str(angle) ]);
2132
       save(name, 'shore')
2133
       % 5. Calculate the area of the shoreline:
2134
       basin = zeros(row,col);
2135
       X = []; % determine the X,Y dimensions of the basin:
2136
       Y = [];
2137
       [rn,cn] = size(basin);
2138
       for j = 1:cn
2139
           X(1:rn,j) = 1:rn;
2140
           Y(1:rn,j) = j;
2141
       end
2142
       y=shore(1,:);
2143
       x = shore(2, :);
2144
       IN=inpolygon(X,Y,x,y); %this returns the logical "IN" matrix which is the
2145
       % same size as X and Y with 1=yes this cell is within the shape, 0=no
2146
       % this cell is outside the shape.
2147
       IN=+IN; %turns logical to numeric
2148
       FluvSurface{i}=IN;
2149
       total=sum(sum(IN));
```

```
2150
       areapix{i}=total;
2151
       DeltaArea = (total*(25*25))/(1000*1000);% This is the area of the Delta [km^2]
2152
2153
       %
          6.
               Calculate the perimeter of the shoreline:
2154
       sizextemp = size(x);
2155
       sizex = sizextemp(2);
2156
       Perimeter = 0;
2157
       dist = zeros(1, sizex);
2158
       for k = 1:sizex-1;
2159
           distx(k) = abs(x(k)*25 - x(k+1)*25);  horizontal distance [m]
2160
           disty(k) = abs(y(k)*25 - y(k+1)*25);  vertical distance [m]
2161
           if distx(k) == 0;
2162
               dist(k) = disty(k);
2163
           end
2164
           if disty(k) == 0;
2165
               dist(k) = distx(k);
2166
           end
2167
           if distx(k) ~= 0;
2168
               if disty(k) ~=0;
2169
                   dist(k) = sqrt(distx(k)^2 + disty(k)^2);
2170
               end
2171
           end
2172
           Perimeter = Perimeter + dist(k); % Perimeter recorded in [m]
2173
       end
2174
       % Add in the distance along the beach!!!
2175
       DistBeach = abs(x(1)*25-x(sizex)*25);
2176
       PerimeterKM = (DistBeach+Perimeter)/1000 % Perimeter length [km]
2177
       % 7. Calculate the dimensionless Isoperimetric Quotient(IQ):
2178
       IQ(i) = (PerimeterKM^2)/(4*pi*DeltaArea)
2179
       Results.Area(1,i)=DeltaArea;
2180
       Results.Perimeter(1,i)=PerimeterKM;
2181
       Results.IQ(1,i)=IQ(i);
2182
       end
2183
       save('FluvialSurface','FluvSurface')
2184
       save('Results','Results')
2185
       save('areapix','areapix')
2186
       % 8. Plot IQ through time:
2187
       figure(2)
2188
       plot(IQ)
2189
       axis([0 tmax 0 1]);
2190
       xlabel('Time Step');
2191
       ylabel('Isoperimetric Quotient');
2192
2193
2194
2195
2196
```

2198	
2199	
2200	Appendix C
2201	
2202	Delft3D-Generated Internal Geometry of Simulated Deltas







4m deep basin, 0mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.







4m deep basin, 5mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



4m deep 10mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



4m deep basin, 10mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



8m deep basin, 0mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.





8m deep basin, 5mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



8m deep 10mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



8m deep basin, 10mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.







12m deep basin, 0mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



12m deep 5mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



12m deep basin, 5mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



12m deep 10mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



12m deep basin, 10mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



20m deep 0mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



20m deep basin, 0mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



20m deep 5mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



20m deep basin, 5mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.



20m deep 10mm/yr RBLF. Upper image is Delft3D stratigraphy strike line with color The bottom image shows the topset(green) and foreset(pink). representing D50 grain size. Yellow is coarse and pink is fine. Black lines represent chronostratigraphic surfaces.



20m deep basin, 10mm/yr RBLF. Dip Line. Black lines are chronostratigraphic surfaces. Color indicates D<sub>50</sub> grain size. Yellow is coarse and pink is fine.

2227	Appendix D
2228	
2229	Processed and Interpreted Ground Penetrating Radar Data
2230	From the Goose River Delta, Labrador, Canada
2231	












## Aug4 Line32 Processing: Dewowed, Bandpass Filtered, F-K(Stolt) Migration (v=0.6n/s), Depth Conversion Clinoforms identified in blue

























































